### WASHINGTON STATE ENERGY CODE, APPENDIX CHAPTERS

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# Appendix A DEFAULT HEAT LOSS COEFFICIENTS

#### SECTION A101 GENERAL REQUIREMENTS

**A101.1 Scope.** The following defaults shall apply to Chapter 4 of both the (RE) and (CE) sections of the WSEC. This chapter includes tables of seasonal average heat loss coefficients for specified nominal insulation.

**A101.2 Description.** These coefficients were developed primarily from data and procedures from the ASHRAE Fundamentals Handbook.

Coefficients not contained in this chapter may be computed using the procedures listed in this reference if the assumptions in the following sections are used, along with data from the sources referenced above.

**A101.3 Air films.** Default R-values used for air films shall be as follows:

#### **<u>R-Value</u>** Condition

0.17 All exterior surfaces

- 0.61 Interior horizontal surfaces, heat flow up
- 0.92 Interior horizontal surfaces, heat flow down
- 0.68 Interior vertical surfaces

**A101.4 Compression of Insulation:** Insulation which is compressed shall be rated in accordance with Table A101.4 or reduction in value may be calculated in accordance with the procedures in the ASHRAE Fundamentals Handbook.

**A101.5 Building materials.** Default R-values used for building materials shall be as shown in Table A101.5.

				Insu	ation R-V	Values at S	Standard T	hickness					
Rated H	R-Value	82	71	60	49	38	30	22	21	19	15	13	11
Stan Thicknes	dard ss, Inches	26.0	22.5	19.0	15.5	12"	9.5	6.5	5.5	6	3.5	3.5	3.5
Nominal Lumber Sizes, Inches	Actual Depth of Cavity, Inches		_	]	nsulation	R-Values	When Ins	stalled in a	Confined	Cavity	_	_	
Truss	26.0	82											—
Truss	22.5		71										—
Truss	19.0	_		60		_			_				—
Truss	15.5	_			49	_			_				—
Truss	12.0	_				38			_				
2x12	11.25					37			_				—
2x10	9.25					32	30		_				—
2x8	7.25	_				27	26	22	21	19	_	_	—
2x6	5.5	_					21	20	21	18			
2x4	3.5							14		13	15	13	11
	2.5											9.8	
	1.5											6.3	6.0

#### TABLE A101.4 R-VALUE OF FIBERGLASS BATTS COMPRESSED WITHIN VARIOUS DEPTH CAVITIES

Material	Nominal Size (in.)	Actual Size (in.)	<b>R-Value</b> (Heat Capacity <sup>3</sup> )
Air cavity (unventilated), between metal studs at 16 inches on center <sup>a</sup>	-	-	0.79
Air cavity (unventilated), all other depths and framing materials <sup>1</sup>	-	-	0.91
Airfilm, exterior surfaces <sup>2</sup>	-	-	0.17
Airfilm, interior horizontal surfaces, heat flow up <sup>2</sup>	_	-	0.61
Airfilm, interior horizontal surfaces, heat flow down <sup>2</sup>	_	_	0.92
Airfilm, interior vertical surfaces <sup>2</sup>	_	-	0.68
Brick at R-0.12/in. (face brick, 75% solid/25% core area, 130 lbs/ft <sup>3</sup> )	4	3.5	
	4	5.5	0.32 (5.9)
Carpet and rubber pad	-	-	1.23
Concrete at R-0.0625/in., heavyweight (144 lbs/ft <sup>3</sup> )	-	2 4	0.13 (HC-4.8)
	-	4 6	0.25 (HC-9.6) 0.38 (HC-14.4)
	_	8	0.50 (HC-19.2)
	_	10	0.63 (HC-24.0)
	_	10	0.75 (HC-28.8)
Concrete masonry units, solid grouted, lightweight (95 lbs/ft3)	6	-	0.80 (HC-11.4)
Concrete masonry units, solid grouted, normal weight (135 lbs/ft3)	6	-	0.51 (HC-13.2)
Concrete masonry units, partly grouted, lightweight (95 lbs/ft3)	6	-	1.33 (HC-6.7)
Concrete masonry units, partly grouted, normal weight (135 lbs/ft3)	6	-	0.82 (HC-9.0)
Concrete masonry units, solid grouted, lightweight (95 lbs/ft3)	8	-	1.05 (HC-15.5)
Concrete masonry units, solid grouted, normal weight (135 lbs/ft3)	8	-	0.69 (HC-17.9)
Concrete masonry units, partly grouted, lightweight (95 lbs/ft3)	8	-	1.44 (HC-9.6)
Concrete masonry units, partly grouted, normal weight (135 lbs/ft3)	8	-	0.98 (HC-12.0)
Concrete masonry units, solid grouted, lightweight (95 lbs/ft3)	10	-	1.30 (HC-19.7)
Concrete masonry units, solid grouted, normal weight (135 lbs/ft3)	10	-	0.87 (HC-22.6)
Concrete masonry units, partly grouted, lightweight (95 lbs/ft3)	10	-	1.61 (HC-11.9)
Concrete masonry units, partly grouted, normal weight (135 lbs/ft3)	10	-	1.11 (HC-14.8)
Concrete masonry units, solid grouted, lightweight (95 lbs/ft3)	12	-	1.53 (HC-23.9)
Concrete masonry units, solid grouted, normal weight (135 lbs/ft3)	12	-	1.06 (HC-27.2)
Concrete masonry units, partly grouted, lightweight (95 lbs/ft3)	12	-	1.75 (HC-14.2)
Concrete masonry units, partly grouted, normal weight (135 lbs/ft3)	12	-	1.23 (HC-17.5)
Flooring, wood subfloor	-	0.75	0.94
Gypsum board	-	0.5	0.45
	-	0.625	0.56
Metal deck	-	-	0
Roofing, built-up	-	0.375	0.33
Sheathing, vegetable fiber board, 0.78 in.	-	0.78	2.06
Soil at R-0.104/in.	-	12	1.25
Steel, mild		1	0.0031807
Stucco	-	0.75	0.08

#### TABLE A101.5 DEFAULT R-VALUES FOR BUILDING MATERIALS

a. There is no credit for cavities that are open to outside air.

b. Air films do not apply to air cavities within an assembly.

c. For heat capacity for concrete and concrete masonry materials with densities other than the values listed in Table A101.5, see Tables A3.1B and A3.1C in ASHRAE/IESNA Standard 90.1.

#### SECTION A102 CEILINGS

**A102.1 General.** Table A102.1 lists heat loss coefficients for the opaque portion of exterior ceilings below vented attics, vaulted ceilings and roof decks in units of Btu/h  $\times$  ft<sup>2</sup>  $\times$  °F of ceiling.

They are derived from procedures listed in the ASHRAE Fundamentals Handbook. Ceiling U-factors are modified for the buffering effect of the attic, assuming an indoor temperature of 65°F and an outdoor temperature of 45°F.

**A102.1.1 Metal framed ceilings.** The nominal R-values in Table A103.3.6.2: Effective R-Values for Metal Framing and Cavity Only may be used for purposes of calculating metal framed ceiling section U-factors in lieu of the ASHRAE zone calculation method as provided in Chapter 27 of the ASHRAE Fundamentals Handbook.

Metal building roofs have a different construction and are addressed in Table A102.2.5.

**A102.2 Component description.** The four types of ceilings are characterized as follows:

A102.2.1 Ceilings below a vented attic. Attic insulation is assumed to be blown-in, loose-fill fiberglass with a K-value of 2.6 h × ft<sup>2</sup> •× °F/Btu per inch. Full bag count for specified R-value is assumed in all cases. Ceiling dimensions for flat ceiling calculations are 45 by 30 feet, with a gabled roof having a 4/12 pitch. The attic is assumed to vent naturally at the rate of 3 air changes per hour through soffit and ridge vents. A void fraction of 0.002 is assumed for all attics with insulation baffles. Standard-framed, unbaffled attics assume a void fraction of 0.008.

Attic framing is either standard or advanced. Standard framing assumes tapering of insulation depth around the perimeter with resultant decrease in thermal resistance. An increased R-value is assumed in the center of the ceiling due to the effect of piling leftover insulation. Advanced framing assumes full and even depth of insulation extending to the outside edge of exterior walls. Advanced framing does not change from the default value. U-factors for flat ceilings below vented attics with standard framing may be modified with the following table:

Roof Pitch	U-fact Standard	or for Framing
	R-30	R-38
4/12	0.036	0.031
5/12	0.035	0.030
6/12	0.034	0.029
7/12	0.034	0.029
8/12	0.034	0.028
9/12	0.034	0.028
10/12	0.033	0.028
11/12	0.033	0.027
12/12	0.033	0.027

Vented scissors truss attics assume a ceiling pitch of 2/12 with a roof pitch of either 4/12 or 5/12. Unbaffled standard framed scissors truss attics are assumed to have a void fraction of 0.016.

**A102.2.2 Vaulted ceilings.** Insulation is assumed to be fiberglass batts installed in roof joist cavities. In the vented case, at least 1.5 inches between the top of the batts and the underside of the roof sheathing is left open for ventilation in each cavity. A ventilation rate of 3.0 air changes per hour is assumed. In the unvented or dense pack case, the ceiling cavity is assumed to be fully packed with insulation, leaving no space for ventilation.

**A102.2.3 Roof decks.** Rigid insulation is applied to the top of roof decking with no space left for ventilation. Roofing materials are attached directly on top of the insulation. Framing members are often left exposed on the interior side.

A102.2.4 Metal truss framing. Overall system tested values for the roof/ceiling  $U_o$  for metal framed truss assemblies from approved laboratories shall be used, when such data is acceptable to the building official.

Alternatively, the  $U_o$  for roof/ceiling assemblies using metal truss framing may be obtained from Tables A102.2.4(1) through A102.2.4(5).

#### TABLE A102.1 DEFAULT U-FACTORS FOR CEILINGS

	Standard Frame	Advanced Frame
Ceilings Below Vented Attics		
Flat	В	Baffled
R-19	0.049	0.047
R-30	0.036	0.032
R-38	0.031	0.026
R-49	0.027	0.020
R-60	0.025	0.017
Scissors Truss		
R-30 (4/12 roof pitch)	0.043	0.031
R-38 (4/12 roof pitch)	0.040	0.025
R-49 (4/12 roof pitch)	0.038	0.020
R-30 (5/12 roof pitch)	0.039	0.032
R-38 (5/12 roof pitch)	0.035	0.026
R-49 (5/12 roof pitch)	0.032	0.020
Vaulted Ceilings	16" O.C.	24" O.C.
Vented		
R-19 2x10 joist	0.049	0.048
R-30 2x12 joist	0.034	0.033
R-38 2x14 joist	0.027	0.027
Unvented		
R-30 2x10 joist	0.034	0.033
R-38 2x12 joist	0.029	0.027
R-21 + R-21 2x12 joist	0.026	0.025
Roof Deck	4x Bea	ms, 48" O.C.
R-12.5 2" Rigid insulation		0.064
R-21.9 3.5" Rigid insulation		0.040
R-37.5 6" Rigid insulation		0.025
R-50 8" Rigid insulation		0.019

# TABLE A102.2.4(1) STEEL TRUSS $^{\rm a}$ FRAMED CEILING U\_o

Cavity						Truss	Span	(ft)					
R-value	12	14	16	18	20	22	24	26	28	30	32	34	36
19	0.1075	0.0991	0.0928	0.0878	0.0839	0.0807	0.0780	0.0757	0.0737	0.0720	0.0706	0.0693	0.0681
30	0.0907	0.0823	0.0760	0.0710	0.0671	0.0638	0.0612	0.0589	0.0569	0.0552	0.0538	0.0525	0.0513
38	0.0844	0.0759	0.0696	0.0647	0.0607	0.0575	0.0548	0.0525	0.0506	0.0489	0.0474	0.0461	0.0449
49	0.0789	0.0704	0.0641	0.0592	0.0552	0.0520	0.0493	0.0470	0.0451	0.0434	0.0419	0.0406	0.0395

# TABLE A102.2.4(2) STEEL TRUSS<sup>a</sup> FRAMED CEILING $U_0$ WITH R-3 SHEATHING

Cavity						Truss	Span	(ft)					
R-value	12	14	16	18	20	22	24	26	28	30	32	34	36
19	0.0809	0.0763	0.0728	0.0701	0.0679	0.0661	0.0647	0.0634	0.0623	0.0614	0.0606	0.0599	0.0592
30	0.0641	0.0595	0.0560	0.0533	0.0511	0.0493	0.0478	0.0466	0.0455	0.0446	0.0438	0.0431	0.0424
38	0.0577	0.0531	0.0496	0.0469	0.0447	0.0430	0.0415	0.0402	0.0392	0.0382	0.0374	0.0367	0.0361
49	0.0523	0.0476	0.0441	0.0414	0.0393	0.0375	0.0360	0.0348	0.0337	0.0328	0.0319	0.0312	0.0306

### TABLE A102.2.4(3)STEEL TRUSS<sup>a</sup> FRAMED CEILING Uo WITH R-5 SHEATHING

Cavity						Truss	Span	(ft)					
R-value	12	14	16	18	20	22	24	26	28	30	32	34	36
19	0.0732	0.0697	0.0670	0.0649	0.0633	0.0619	0.0608	0.0598	0.0590	0.0583	0.0577	0.0571	0.0567
30	0.0564	0.0529	0.0502	0.0481	0.0465	0.0451	0.0440	0.0430	0.0422	0.0415	0.0409	0.0403	0.0399
38	0.0501	0.0465	0.0438	0.0418	0.0401	0.0388	0.0376	0.0367	0.0359	0.0351	0.0345	0.0340	0.0335
49	0.0446	0.0410	0.0384	0.0363	0.0346	0.0333	0.0322	0.0312	0.0304	0.0297	0.0291	0.0285	0.0280

TABLE A102.2.4(4) STEEL TRUSS<sup>a</sup> FRAMED CEILING U<sub>o</sub> WITH R-10 SHEATHING

Cavity						Truss	Span	(ft)					
R-value	12	14	16	18	20	22	24	26	28	30	32	34	36
19	0.0626	0.0606	0.0590	0.0578	0.0569	0.0561	0.0555	0.0549	0.0545	0.0541	0.0537	0.0534	0.0531
30	0.0458	0.0437	0.0422	0.0410	0.0401	0.0393	0.0387	0.0381	0.0377	0.0373	0.0369	0.0366	0.0363
38	0.0394	0.0374	0.0359	0.0347	0.0337	0.0330	0.0323	0.0318	0.0313	0.0309	0.0305	0.0302	0.0299
49	0.0339	0.0319	0.0304	0.0292	0.0283	0.0275	0.0268	0.0263	0.0258	0.0254	0.0251	0.0247	0.0245

TABLE A102.2.4(5) STEEL TRUSS<sup>a</sup> FRAMED CEILING U<sub>o</sub> WITH R-15 SHEATHING

Cavity						Truss	Span	(ft)					
R-value	12	14	16	18	20	22	24	26	28	30	32	34	36
19	0.0561	0.0550	0.0541	0.0535	0.0530	0.0526	0.0522	0.0519	0.0517	0.0515	0.0513	0.0511	0.0509
30	0.0393	0.0382	0.0373	0.0367	0.0362	0.0358	0.0354	0.0351	0.0349	0.0347	0.0345	0.0343	0.0341
38	0.0329	0.0318	0.0310	0.0303	0.0298	0.0294	0.0291	0.0288	0.0285	0.0283	0.0281	0.0279	0.0278
49	0.0274	0.0263	0.0255	0.0249	0.0244	0.0239	0.0236	0.0233	0.0230	0.0228	0.0226	0.0225	0.0223

Footnotes for Tables A102.2.4(1) through A102.2.4(5)

a. Assembly values based on 24 inch on center truss spacing; 11 Truss member connections penetrating insulation (4 at the eaves, 7 in the interior space); ½ inch drywall ceiling; all truss members are 2x4 "C" channels with a solid web.

b. Ceiling sheathing installed between bottom chord and drywall.

**A102.2.5 Metal building roof.** Table A102.2.5: The base assembly is a roof where the insulation is compressed when installed beneath metal roof panels attached to the steel structure (purlins). Additional assemblies include continuous insulation, uncompressed and uninterrupted by framing.

U-factors for metal building roofs shall be taken from Table A102.2.5, provided the average purlin spacing is at least 52 inches and the R-value of the thermal spacer block is greater than or equal to the thermal spacer block R-value indicated in Table A107.2.5 for the assembly. It is not acceptable to use the U-factors in Tables A102.2.6(1), A102.2.6(2) or A102.2.6(3) if additional insulated sheathing is not continuous. **A102.2.5.1 Single layer.** The rated R-value of insulation is for insulation installed perpendicular to and draped over purlins and then compressed when the metal roof panels are attached. A minimum R-3 (R-0.5) thermal spacer block between the purlins and the metal roof panels is required, unless compliance is shown by the overall assembly U-factor.

**A102.2.5.2 Double layer.** The first rated R-value of insulation is for insulation installed perpendicular to and draped over purlins. The second rated R-value of insulation is for unfaced insulation installed above the first layer and parallel to the purlins and then compressed when the metal roof panels are attached. A minimum R-3 (R-0.5) thermal spacer block between the purlins and the metal roof panels is required, unless compliance is shown by the overall assembly U-factor.

A102.2.5.3 Continuous insulation. For

continuous insulation (e.g., insulation boards or blankets), it is assumed that the insulation is installed below the purlins and is uninterrupted by framing members. Insulation exposed to the conditioned space or semi-heated space shall have a facing, and all insulation seams shall be continuously sealed to provide a continuous air barrier.

A102.2.5.4 Liner system (Ls). A continuous membrane is installed below the purlins and uninterrupted by framing members. Uncompressed, unfaced insulation rests on top of the membrane between the purlins. For multilayer installations, the last rated R-value of insulation is for unfaced insulation draped over purlins and then compressed when the metal roof panels are attached. A minimum R-3 (R-0.5) thermal spacer block between the purlins and the metal roof panels is required, unless compliance is shown by the overall assembly U-factor.

A102.2.5.5 Filled cavity. The first rated Rvalue of insulation is for faced insulation installed parallel to the purlins. The second rated R-value of insulation is for unfaced insulation installed above the first layer, parallel to and between the purlins and compressed when the metal roof panels are attached. The facer of the first layer of insulation is of sufficient width to be continuously sealed to the top flange of the purlins and to accommodate the full thickness of the second layer of insulation. A supporting structure retains the bottom of the first layer at the prescribed depth required for the full thickness of the second layer of insulation being installed above it. A minimum R-5 (R-0.9) thermal spacer block between the purlins and the metal roof panels is required, unless compliance is shown by the overall assembly U-factor.

A102.2.6 Roofs with insulation entirely above deck (uninterrupted by framing). Table A102.2.6(1) through A102.2.6(3): The base assembly is continuous insulation over a structural deck. These tables indicate effective U-factors for tapered roof insulation, sloped from a maximum R-value ( $R_{max}$ ) at the peak of the slope to a minimum R-value ( $R_{min}$ ) at the low point of the slope. The rows of the tables represent the rated R-value of the insulation at the minimum conditions (except at roof drains) and the columns of the table represent the rated R-value of the insulation at the maximum conditions. The slope of the tapered insulation shall be no greater than 1/4 inch per foot.

TABLE A102.2.5
DEFAULT U-FACTORS FOR METAL BUILDING ROOFS

Insulation System	Rated R-Value of Insulation	Overall U-Factor for Entire Base	Overall U-Factor for Assembly of Base Roof Plus Continuous Insulation (uninterrupted by framing) Rated R-Value of Continuous Insulation							
ojstem	of mountain	Roof Assembly	R-6.5	R-13	R-19.5	R-26	R-32.5	R-39		
Standing Sea	am Roofs with Ther	mal Spacer Blocks <sup>a,b</sup>								
Single	None	1.280	0.137	0.073	0.049	0.037	0.030	0.025		
Layer	R-10	0.115	0.066	0.046	0.035	0.029	0.024	0.021		
	R-11	0.107	0.063	0.045	0.035	0.028	0.024	0.021		
	R-13	0.101	0.061	0.044	0.034	0.028	0.024	0.020		
	R-16	0.096	0.059	0.043	0.033	0.027	0.023	0.020		
	R-19	0.082	0.053	0.040	0.031	0.026	0.022	0.020		
Double	R-10.+R-10	0.088	0.056	0.041	0.032	0.027	0.023	0.020		
Layer	R-10.+R-11	0.086	0.055	0.041	0.032	0.027	0.023	0.020		
	R-11 .+ R-11	0.085	0.055	0.040	0.032	0.026	0.023	0.020		
	R-10 .+ R-13	0.084	0.054	0.040	0.032	0.026	0.023	0.020		
	R-11 .+ R-13	0.082	0.053	0.040	0.032	0.026	0.022	0.020		
	R-13 .+ R-13	0.075	0.050	0.038	0.030	0.025	0.022	0.019		
	R10.+R-19	0.074	0.050	0.038	0.030	0.025	0.022	0.019		
	R-11 .+ R-19	0.072	0.049	0.037	0.030	0.025	0.022	0.019		
	R-13 .+ R-19	0.068	0.047	0.036	0.029	0.025	0.021	0.019		
	R-16 .+ R-19	0.065	0.046	0.035	0.029	0.024	0.021	0.018		
	R-19 .+ R-19	0.060	0.043	0.034	0.028	0.023	0.020	0.018		
Liner	R-19 .+ R-11	0.035								
System	R-25 .+ R-11	0.031								
	R-30 .+ R-11	0.029								
	R-25 .+ R-11 .+ R-11	0.026								
Filled Cavity	y with Thermal Spa	cer Blocks <sup>c</sup>								
	R-10 .+ R-19	0.057	0.042	0.033	0.027	0.023	0.020	0.018		
Standing Se	am Roofs without T	hermal Spacer Blocks								
Liner System	R-19 .+ R-11	0.040								
Thru-Faster	ed Roofs without T	hermal Spacer Blocks		•						
Single	R-10	0.184								
Layer	R-11	0.182								
	R-13	0.174	1					1		
	R-16	0.157								
	R-10	0.157								
Liner System	R-19 .+ R-11	0.044								

(Multiple R-values are listed in order from inside to outside)

a. A standing seam roof clip that provides a minimum 1.5 in. distance between the top of the purlins and the underside of the metal roof panels is required.

b. A minimum R-3 thermal spacer block is required.

c. A minimum R-5 thermal spacer block is required.

	SINGLE SLOPE RECTANGULAR TO ONE-SIDE <sup>,d,f,g,h,i</sup> (UNINTERRUPTED BY FRAMING)													
			Rated R-Value of Insulation at M aximum Condition (Rmax <sup>1</sup> )											
		1	5	10	15	20	25	30	35	40	45	50	55	60
E	1	0.562	0.306	0.213	0.168	0.140	0.121	0.107	0.097	0.088	0.081	0.075	0.070	0.066
Minimum	5	-	0.173	0.125	0.101	0.086	0.076	0.068	0.062	0.057	0.053	0.049	0.046	0.044
	10	-	-	0.093	0.076	0.066	0.058	0.053	0.048	0.045	0.042	0.039	0.037	0.035
	15	-	-	-	0.063	0.055	0.049	0.045	0.041	0.038	0.036	0.034	0.032	0.030
llation a (Rmin <sup>+</sup> )	20	-	-	-	-	0.048	0.043	0.039	0.036	0.034	0.032	0.030	0.028	0.027
ja P	25		1	1	I	-	0.039	0.035	0.033	0.031	0.029	0.027	0.026	0.025
	30					-	-	0.032	0.030	0.028	0.026	0.025	0.024	0.023
, 2÷≦	35					-	-	-	0.028	0.026	0.025	0.023	0.022	0.021
value of Insi Condition	40					-	-	-	-	0.025	0.023	0.022	0.021	0.020
	45			+		-	-	-	-	-	0.022	0.021	0.020	0.019
d B	50					-	-	-	-	-	-	0.020	0.019	0.018
Rated R-	55	-	-	-	-	-	-	-	-	-	-	-	0.018	0.017
E	60	-	-	-	-	-	-	-	-	-	-	-	-	0.016

# TABLE A102.2.6(1) ASSEMBLY U-FACTORS FOR ROOFS WITH TAPERED INSULATION ENTIRELY ABOVE DECK

### TABLE A102.2.6(2) ASSEMBLY U-FACTORS FOR ROOFS WITH TAPERED INSULATION ENTIRELY ABOVE DECK SLOPED TRIANGLE (ROOF WITH CENTER DRAIN)<sup>e,f,g,h,i</sup> (UNINTERRUPTED BY FRAMING)

				Ra	ted R-V	alue of I	nsulatio	n at M a	xim um C	onditio	n (Rmax	<sup>2</sup> )		
		1	5	10	15	20	25	30	35	40	45	50	55	60
E	1	0.562	0.242	0.146	0.106	0.083	0.068	0.058	0.051	0.045	0.040	0.036	0.033	0.031
Ē	5	-	0.173	0.112	0.084	0.068	0.057	0.049	0.044	0.039	0.035	0.032	0.030	0.028
Minimum	10	-	-	0.093	0.071	0.059	0.050	0.044	0.039	0.035	0.032	0.029	0.027	0.025
	15	-	-	-	0.063	0.053	0.045	0.040	0.035	0.032	0.029	0.027	0.025	0.023
ulation a (Rmin <sup>2</sup> )	20				0.048	0.042	0.037	0.033	0.030	0.027	0.025	0.024	0.022	
ulation (Rmin <sup>†</sup>	25					-	0.039	0.034	0.031	0.028	0.026	0.024	0.022	0.021
	30					-	-	0.032	0.029	0.027	0.025	0.023	0.021	0.020
due of Inst Condition	35		1			-	-	-	0.028	0.026	0.024	0.022	0.021	0.019
e 5	40		→ >	< ←	_	-	-	-	-	0.025	0.023	0.021	0.020	0.019
R-value Cor	45		1			-	-	-	-	-	0.022	0.020	0.019	0.018
ц Ч Ц Ц Ц	÷ 50				-	-	-	-	-	-	0.020	0.018	0.017	
Bated	55					-	-	-	-	-	-	-	0.018	0.017
ш	60					-	-	-	-	-	-	-	-	0.016

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#### TABLE A102.2.6(3) ASSEMBLY U-FACTORS FOR ROOFS WITH TAPERED INSULATION ENTIRELY ABOVE DECK SLOPED TRIANGLE (ROOF WITH PERIMETER DRAINS)<sup>e,f,g,h,i</sup> (UNINTERRUPTED BY FRAMING)

			Rated R-Value of Insulation at Maximum Condition (Rmax <sup>3</sup> )											
		1	5	10	15	20	25	30	35	40	45	50	55	60
E	1	0.562	0.363	0.273	0.224	0.193	0.170	0.153	0.139	0.128	0.119	0.111	0.105	0.099
Ē	5	-	0.173	0.138	0.118	0.104	0.094	0.086	0.079	0.074	0.070	0.066	0.062	0.059
Minimum	10	-	-	0.093	0.081	0.073	0.067	0.062	0.058	0.054	0.051	0.049	0.046	0.044
			-	0.063	0.058	0.053	0.050	0.047	0.044	0.042	0.040	0.038	0.037	
					0.048	0.045	0.042	0.040	0.037	0.036	0.034	0.033	0.032	
ja E						-	0.039	0.037	0.035	0.033	0.031	0.030	0.029	0.028
nst n	30					-	-	0.032	0.031	0.029	0.028	0.027	0.026	0.025
llee of Ins Condition	35			1		-	-	-	0.028	0.027	0.026	0.025	0.024	0.023
<b>≗</b> 5	40	-	-	$\times -$	-	-	-	-	-	0.025	0.024	0.023	0.022	0.021
	45		/			-	-	-	-	-	0.022	0.021	0.020	0.020
	<b>É</b> 50				-	-	-	-	-	-	0.020	0.019	0.019	
Bated	55		+			-	-	-	-	-	-	-	0.018	0.017
<b>•</b>	60					-	-	-	-	-	-	-	-	0.016

#### Footnotes to Tables A102.2.6.1, A102.2.6.2, and A102.2.6.3:

- a. R<sub>max</sub> and R<sub>min</sub> are determined along the linearly tapered cross section for the respective minimum and maximum thickness values for the roof section being analyzed. For triangular roof sections
- b.  $R_{max}$  refers to the insulation value along the long edge of the triangle and  $R_{min}$  to the insulation at the point of the triangle which assumes that the insulation slopes to the center.
- c.  $R_{max}$  refers to the insulation value at the point of the triangle and  $R_{min}$  to the insulation along the long edge of the triangle which assumes that the insulation slopes to the perimeter.
- d. Effective U-factor for rectangular tapered insulation is calculated as follows: R

$$eff = \frac{R_{\max} - R_{\min}}{\ln \left[\frac{R_{\max}}{R_{\min}}\right]}$$

e. Effective U-factor for triangular tapered insulation is calculated as follows:

$$R_{eff} = \left[\frac{2}{R_{\max} - R_{\min}} \left[1 + \frac{R_{\min}}{R_{\max} - R_{\min}} \ln\left(\frac{R_{\min}}{R_{\max}}\right)\right]\right]^{-1}$$

- f. Assembly U-factors include an exterior air film (R=0.17) and an interior air film, horizontal with heat flow up (R=0.61).
- g. For effective U-factors of roof assemblies with different  $R_{max}$  or  $R_{min}$  values not listed in the tables interpolation is allowed.
- h. This table shall only be applied to tapered insulation that is tapered along only one axis.
- i. In areas of differing insulation slopes/configurations, individual U-values shall be calculated and an area weighted U-value calculation shall be used to determine the effective value of the roof.

#### SECTION A103 ABOVE GRADE WALLS

**A103.1 General.** The tables in this section list heat loss coefficients for the opaque portion of abovegrade wood stud frame walls, metal stud frame walls and concrete masonry walls (Btu/h  $\times$  ft<sup>2</sup>  $\times$  °F). They are derived from procedures listed in the ASHRAE Fundamentals Handbook. For intermediate floor slabs which penetrate the insulated wall, use the concrete wall U-factors in Table A103.3.7.1(1).

Insulation is assumed to uniformly fill the entire cavity and to be installed as per manufacturer's directions. All walls are assumed to be finished on the inside with 1/2 inch gypsum wallboard, and on the outside with either beveled wood siding over 1/2 inch plywood sheathing or with 5/8 inch T1-11 siding. Insulated sheathing (either interior or exterior) is assumed to cover the entire opaque wall surface, except where modified in accordance with footnote g to Table C402.1.3.

Metal building walls have a different construction and are addressed in Table A103.3.6.3.

**A103.2 Framing description.** For wood stud frame walls, three framing types are considered and defined as follows:

**A103.2.1 Standard.** Studs framed on 16 inch centers with double top plate and single bottom plate. Corners use three studs and each opening is framed using two studs. Headers consist of double 2x or single 4x material with an air space left between the header and the exterior sheathing. Interior partition wall/exterior wall intersections use two studs in the exterior wall.

#### Standard framing weighting factors:

Studs and plates	0.19
Insulated cavity	0.77
Headers	0.04

**A103.2.2 Intermediate.** Studs framed on 16 inch centers with double top plate and single bottom plate. Corners use two studs or other means of fully insulating corners, and each opening is framed by two studs. Headers consist of double 2x material with R-10 insulation. Interior partition wall/exterior wall intersections are fully insulated in the exterior wall.

#### Intermediate framing weighting factors:

Studs and plates	0.18
Insulated cavity	0.78
Headers	0.04

**A103.2.3 Advanced.** Studs framed on 24 inch centers with double top plate and single bottom plate. Corners use two studs or other means of fully insulating corners, and one stud is used to support each header. Headers consist of double 2x material with R-10 insulation. Interior partition wall/exterior wall intersections are fully insulated in the exterior wall.

#### Advanced framing weighting factors:

Studs and plates	0.13
Insulated cavity	0.83
Headers	0.04

**A103.3 Component description.** Default coefficients for the following types of walls are listed: Single-stud walls, strap walls, double-stud walls, log walls, stress-skin panels, metal stud walls, and metal building walls.

A103.3.1 Single-stud wall. Tables A103.3.1(1) through A103.3.1(8): Assumes either  $2 \times 4$  or  $2 \times 6$  studs framed on 16 or 24 inch centers. Headers are solid for  $2 \times 4$  walls and double  $2 \times$  for  $2 \times 6$  walls, with either dead-air or rigid-board insulation in the remaining space.

#### TABLE A103.3.1(1) 2 x 4 Single Wood Stud: R-11 Batt

NOTE: Nominal Batt R-value: R-11 at 3.5 inch thickness

Installed Batt R-value: R-11 in 3.5 inch cavity

	Siding Mat	erial/Frami	ng Type	Siding Material/Framing Type											
R-value of	Lapped	d Wood	T1	-11											
Foam Board	STD	ADV	STD	ADV											
0	0.088	0.084	0.094	0.090											
1	0.080	0.077	0.085	0.082											
2	0.074	0.071	0.078	0.075											
3	0.069	0.066	0.072	0.070											
4	0.064	0.062	0.067	0.065											
5	0.060	0.058	0.063	0.061											
6	0.056	0.055	0.059	0.057											
7	0.053	0.052	0.055	0.054											
8	0.051	0.049	0.052	0.051											
9	0.048	0.047	0.050	0.049											
10	0.046	0.045	0.047	0.046											
11	0.044	0.043	0.045	0.044											
12	0.042	0.041	0.043	0.042											

#### TABLE A103.3.1(2) 2 x 4 Single Wood Stud: R-13 Batt

NOTE:

Nominal Batt R-value: R-13 at 3.63 inch thickness

Installed Batt R-value: R-12.7 in 3.5 inch cavity

	Siding Mat	erial/Frami	ng Type	
R-value of	Lapped	Wood	T1-	-11
Foam Board	STD	ADV	STD	ADV
0	0.082	0.078	0.088	0.083
1	0.075	0.072	0.080	0.076
2	0.069	0.066	0.073	0.070
3	0.065	0.062	0.068	0.065
4	0.060	0.058	0.063	0.061
5	0.057	0.055	0.059	0.057
6	0.053	0.052	0.056	0.054
7	0.051	0.049	0.052	0.051
8	0.048	0.047	0.050	0.048
9	0.046	0.045	0.047	0.046
10	0.044	0.043	0.045	0.044
11	0.042	0.041	0.043	0.042
12	0.040	0.039	0.041	0.040

#### TABLE A103.3.1(3) 2 x 4 Single Wood Stud: R-15 Batt

	Sie	ding Materi	al/Framing	Туре	
		Lapped	Wood	T1	-11
NOTE:	R-value of Foam Board	STD	ADV	STD	ADV
Nominal Batt R-value:	0	0.076	0.071	0.081	0.075
R-15 at 3.5 inch thickness	1	0.069	0.065	0.073	0.069
	2	0.064	0.061	0.068	0.069
Installed Batt R-value:	3	0.060	0.057	0.063	0.059
R-15 in 3.5 inch cavity	4	0.056	0.053	0.059	0.056
	5	0.053	0.051	0.055	0.052
	6	0.050	0.048	0.052	0.050
	7	0.047	0.046	0.049	0.047
	8	0.045	0.044	0.047	0.045
	9	0.043	0.042	0.044	0.043
	10	0.041	0.040	0.042	0.041
	11	0.039	0.038	0.041	0.039
	12	0.038	0.037	0.039	0.038

#### TABLE A103.3.1(4) 2 x 6 Single Wood Stud: R-19 Batt

		S	iding Mat	erial/Frami	ing Type		
	R-value of	La	apped Wo	od		T1-11	
NOTE:	Foam Board	STD	INT	ADV	STD	INT	ADV
Nominal Batt R-value:	0	0.062	0.058	0.055	0.065	0.061	0.058
R-19 at 6 inch thickness	1	0.058	0.055	0.052	0.060	0.057	0.055
	2	0.054	0.052	0.050	0.056	0.054	0.051
Installed Batt R-value:	3	0.051	0.049	0.047	0.053	0.051	0.049
R-18 in 5.5 inch cavity	4	0.048	0.046	0.045	0.050	0.048	0.046
	5	0.046	0.044	0.043	0.048	0.046	0.044
	6	0.044	0.042	0.041	0.045	0.044	0.042
	7	0.042	0.040	0.039	0.043	0.042	0.040
	8	0.040	0.039	0.038	0.041	0.040	0.039
	9	0.038	0.037	0.035	0.039	0.038	0.037
	10	0.037	0.036	0.035	0.038	0.037	0.036
	11	0.036	0.035	0.034	0.036	0.035	0.035
	12	0.034	0.033	0.033	0.035	0.034	0.033

#### TABLE A103.3.1(5) 2 x 6 Single Wood Stud: R-21 Batt

		S	iding Mat	erial/Frami	ng Type		
	R-value of	La	apped Wo	od		T1-11	
NOTE:	Foam Board	STD	INT	ADV	STD	INT	ADV
Nominal Batt R-value:	0	0.057	0.054	0.051	0.060	0.056	0.053
R-21 at 5.5 inch thickness	1	0.054	0.051	0.048	0.056	0.053	0.050
	2	0.050	0.048	0.045	0.052	0.050	0.047
Installed Batt R-value:	3	0.048	0.045	0.043	0.049	0.047	0.045
R-21 in 5.5 inch cavity	4	0.045	0.043	0.041	0.047	0.045	0.043
	5	0.043	0.041	0.040	0.044	0.042	0.041
	6	0.041	0.039	0.038	0.042	0.041	0.039
	7	0.039	0.038	0.036	0.040	0.039	0.037
	8	0.038	0.036	0.035	0.039	0.037	0.036
	9	0.036	0.035	0.034	0.037	0.036	0.035
	10	0.035	0.034	0.033	0.036	0.035	0.033
	11	0.033	0.033	0.032	0.034	0.033	0.032
	12	0.032	0.031	0.031	0.033	0.032	0.031

#### TABLE A103.3.1(6) 2 x 6 Single Wood Stud: R-22 Batt

		S	iding Mat	erial/Frami	ng Type			
	R-value of	La	Lapped Wood			T1-11		
NOTE:	Foam Board	STD	INT	ADV	STD	INT	ADV	
Nominal Batt R-value:	0	0.059	0.055	0.052	0.062	0.058	0.054	
R-22 at 6.75 inch thickness	1	0.055	0.052	0.049	0.057	0.054	0.051	
	2	0.052	0.049	0.047	0.054	0.051	0.048	
Installed Batt R-value:	3	0.049	0.046	0.044	0.050	0.048	0.046	
R-20 in 5.5 inch cavity	4	0.046	0.044	0.042	0.048	0.046	0.044	
	5	0.044	0.042	0.041	0.045	0.043	0.042	
	6	0.042	0.040	0.039	0.043	0.042	0.040	
	7	0.040	0.039	0.037	0.041	0.040	0.038	
	8	0.038	0.037	0.036	0.039	0.038	0.037	
	9	0.037	0.036	0.035	0.038	0.037	0.035	
	10	0.035	0.034	0.033	0.036	0.035	0.034	
	11	0.034	0.033	0.032	0.035	0.034	0.033	
	12	0.033	0.032	0.031	0.034	0.033	0.032	

#### TABLE A103.3.1(7) 2 x 6 Single Wood Stud: Two R<u>-11 Batts</u>

		S	iding Mat	erial/Frami	ng Type			
	R-value of	La	Lapped Wood			T1-11		
NOTE:	Foam Board	STD	INT	ADV	STD	INT	ADV	
Nominal Batt R-value:	0	0.060	0.057	0.054	0.063	0.059	0.056	
R-22 at 7 inch thickness	1	0.056	0.053	0.051	0.059	0.056	0.053	
	2	0.053	0.050	0.048	0.055	0.052	0.050	
Installed Batt R-value:	3	0.050	0.048	0.046	0.052	0.049	0.047	
R-18.9 in 5.5 inch cavity	4	0.047	0.045	0.044	0.049	0.047	0.045	
	5	0.045	0.043	0.042	0.046	0.045	0.043	
	6	0.043	0.041	0.040	0.044	0.043	0.041	
	7	0.041	0.040	0.038	0.042	0.041	0.039	
	8	0.039	0.038	0.037	0.040	0.039	0.038	
	9	0.038	0.037	0.036	0.039	0.038	0.036	
	10	0.036	0.035	0.034	0.037	0.036	0.035	
	11	0.035	0.034	0.033	0.036	0.035	0.034	
	12	0.034	0.033	0.032	0.034	0.034	0.033	

#### TABLE A103.3.1(8) 2 x 8 Single Stud: R-25 Batt

J		S	iding Mat	erial/Frami	ng Type		
	R-value of	lue of Lapped Wood			T1-11		
NOTE:	Foam Board	STD	INT	ADV	STD	INT	ADV
Nominal Batt R-value:	0	0.051	0.047	0.045	0.053	0.049	0.046
R-25 at 8 inch thickness	1	0.048	0.045	0.043	0.049	0.046	0.044
	2	0.045	0.043	0.041	0.047	0.044	0.042
Installed Batt R-value:	3	0.043	0.041	0.039	0.044	0.042	0.040
R-23.6 in 7.25 inch cavity	4	0.041	0.039	0.037	0.042	0.040	0.038
	5	0.039	0.037	0.036	0.040	0.038	0.037
	6	0.037	0.036	0.035	0.038	0.037	0.036
	7	0.036	0.035	0.033	0.037	0.035	0.034
	8	0.035	0.033	0.032	0.035	0.034	0.033
	9	0.033	0.032	0.031	0.034	0.033	0.032
	10	0.032	0.031	0.030	0.033	0.032	0.031
	11	0.031	0.030	0.029	0.032	0.031	0.030
	12	0.030	0.029	0.028	0.031	0.030	0.029

**A103.3.2 Strap wall.** Table A103.3.2: Assumes  $2 \ge 6$  studs framed on 16 or 24 inch centers.  $2 \ge 3$  or  $2 \ge 4$  strapping is run horizontally along the interior surface of the wall to provide additional space for insulation.

**A103.3.3 Double stud wall.** Tables A103.3.3(1) and A103.3.3(2): Assumes an exterior structural wall and a separate interior, nonstructural wall.

Insulation is placed in both wall cavities and in the space between the two walls. Stud spacing is assumed to be on 24 inch centers for both walls.

A103.3.4 Log wall. See Table A103.3.4.

A103.3.5 Stress-skin panel. See Table A103.3.5.

#### TABLE A103.3.2 2 X 6: STRAP WALL

	Siding Material/Frame Type						
	Lapped	l Wood	T1-	-11			
	STD						
R-19 + R-11 Batts	0.036	0.035	0.038	0.036			
R-19 + R-8 Batts	0.041	0.040					

#### TABLE A103.3.3(1) 2 X 6 + 2 X 4: DOUBLE WOOD STUD

			Siding Material/Frame Type				
Batt Configuration			Lapped Wood T1-11			-11	
Exterior	Middle	Interior	STD	ADV	STD	ADV	
R-19		R-11	0.040	0.037	0.041	0.038	
R-19		R-19	0.034	0.031	0.035	0.032	
R-19	R-8	R-11	0.029	0.028	0.031	0.029	
R-19	R-11	R-11	0.027	0.026	0.028	0.027	
R-19	R-11	R-19	0.024	0.023	0.025	0.023	
R-19	R-19	R-19	0.021	0.020	0.021	0.020	

#### TABLE A103.3.3(2) 2 X 4 + 2 X 4: DOUBLE WOOD STUD

	-		Siding Material/Frame Type				
Batt Configuration			Lapped	l Wood	T1-11		
Exterior	Middle	Interior	STD	ADV	STD	ADV	
R-11		R-11	0.050	0.046	0.052	0.048	
R-19		R-11	0.039	0.037	0.043	0.039	
R-11	R-8	<b>R-11</b>	0.037	0.035	0.036	0.036	
R-11	R-11	R-11	0.032	0.031	0.033	0.032	
R-13	R-13	R-13	0.029	0.028	0.029	0.028	
R-11	R-19	R-11	0.026	0.026	0.027	0.026	

#### TABLE A103.3.4 LOG WALLS

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NOTE:	Average Log Diameter, Inches	U-factor
R-value of wood:	6	0.148
R-1.25 per inch thickness	8	0.111
	10	0.089
Average wall thickness	12	0.074
90% average log	14	0.063
diameter	16	0.056

**A103.3.6 Metal stud walls.** The nominal R-values in Tables A103.3.6.1 through A103.3.6.3 may be used for purposes of calculating metal stud wall section U-factors in lieu of the ASHRAE zone calculation method as provided in Chapter 27 of the ASHRAE Fundamentals Handbook.

**A103.3.6.1 Metal stud wall, overall assembly U-factors.** Tables A103.3.6.1(1) and A103.6.1(2): Assumes metal studs spaced on 16 or 24 inch centers with insulation installed to fill wall cavities. Continuous rigid board insulation is applied without creating uninsulated voids in the wall assembly.

A103.3.6.2 Metal stud wall, effective R-values for metal framing and cavity only. Table A103.3.6.2: These values may be used for the metal-framing/cavity layers in walls with metal studs spaced on 16- or 24-inch centers with insulation installed to fill wall cavities in lieu of using the zone method provided in Chapter 25 of the ASHRAE Fundamentals Handbook.

**A103.3.6.3 Metal building wall.** Table A103.3.6.3: A wall whose structure consists of metal spanning panels supported by steel structural members (does not include spandrel glass or metal panels in curtain wall systems). The first nominal R-value is for insulation compressed between metal wall panels and the steel structure. For double-layer installations, the second rated R-value of insulation is for insulation installed from the inside, covering the

#### TABLE A103.3.5 STRESS SKIN PANEL

	Panel Thickness, Inches	U-factor
NOTE:		
R-value of expanded	3 1/2	0.071
polystyrene: R-3.85	5 1/2	0.048
per inch	7 1/4	0.037
Framing: 6%	9 1/4	0.030
Spline: 8%	11 1/4	0.025

No thermal bridging between interior and exterior splines

girts. For continuous insulation (e.g., insulation boards) it is assumed that the insulation boards are installed on the inside of the girts and uninterrupted by the framing members. Insulation exposed to the conditioned space or semi-heated space shall have a facing, and all insulation seams shall be continuously sealed to provide a continuous air barrier.

#### A103.3.7 Concrete and masonry walls.

A103.3.7.1 Concrete masonry walls. The nominal R-values in Tables A103.3.7.1(1) and , A103.3.7.1(2) may be used for purposes of calculating concrete masonry wall section Ufactors in lieu of the ASHRAE isothermal planes calculation method as provided in Chapter 27 of the ASHRAE Fundamentals Handbook

A103.3.7.2 Peripheral edges of intermediate concrete floors. See Table A103.3.7.2.

#### TABLE A103.3.6.1(1) OVERALL ASSEMBLY U-FACTORS FOR METAL STUD WALLS WITH CONTINUOUS INSULATION

	R-Value of				sulation		
Metal Framing	Continuous Foam Board Insulation	R-0	R-11	R-13	R-15	R-19	R-21
16" o.c.	R-0 (none)	0.352	0.132	0.124	0.118	0.109	0.106
10 0.0.	· · · ·	0.332			0.118		0.100
	R-1 R-2	0.200	0.117 0.105	0.111 0.100		0.099	0.098
	R-2 R-3	0.207	0.103	0.100	0.096 0.087	0.090	0.087
	R-4	0.146	0.087	0.083	0.080	0.076	0.074
	R-5	0.128	0.080	0.077	0.074	0.071	0.069
	R-6	0.113	0.074	0.071	0.069	0.066	0.065
	R-7	0.102	0.069	0.066	0.065	0.062	0.061
	R-8	0.092	0.064	0.062	0.061	0.058	0.057
	R-9	0.084	0.060	0.059	0.057	0.055	0.054
	R-10	0.078	0.057	0.055	0.054	0.052	0.051
	R-11	0.072	0.054	0.052	0.051	0.050	0.049
	R-12	0.067	0.051	0.050	0.049	0.047	0.047
	R-13	0.063	0.049	0.048	0.047	0.045	0.045
	R-14	0.059	0.046	0.045	0.045	0.043	0.043
	R-15	0.056	0.044	0.043	0.043	0.041	0.041
	R-20	0.044	0.036	0.036	0.035	0.034	0.034
24" o.c	R-0 (none)	0.338	0.116	0.108	0.102	0.094	0.090
	R-1	0.253	0.104	0.098	0.092	0.086	0.083
	R-2	0.202	0.094	0.089	0.084	0.079	0.077
	R-3	0.168	0.086	0.082	0.078	0.073	0.071
	R-4	0.144	0.079	0.075	0.072	0.068	0.066
	R-5	0.126	0.073	0.070	0.067	0.064	0.062
	R-6	0.112	0.068	0.066	0.063	0.060	0.059
	R-7	0.100	0.064	0.062	0.059	0.057	0.055
	R-8	0.091	0.060	0.058	0.056	0.054	0.052
	R-9	0.084	0.057	0.055	0.053	0.051	0.050
	R-10	0.077	0.054	0.052	0.050	0.048	0.048
	R-11	0.072	0.051	0.049	0.048	0.046	0.045
	R-12	0.067	0.048	0.047	0.046	0.044	0.043
	R-13	0.063	0.046	0.045	0.044	0.042	0.042
	R-14	0.059	0.044	0.043	0.042	0.041	0.040
	R-15	0.056	0.042	0.041	0.040	0.039	0.038
	R-20	0.044	0.035	0.034	0.034	0.033	0.032

Continuous foam board insulation: Continuous insulation assumes no thermal bridging of insulation by framing or z-furring through applied foam board. Zone calculation method as provided in the ASHRAE Fundamentals Handbook must be used for thermally bridged foam board insulation. Values for attachment of insulation with z-furring are given in Table A103.3.6.1(2).

#### TABLE A105.3.6.1(2) OVERALL ASSEMBLY U-FACTORS FOR METAL STUD WALLS WITH INSULATION SUPPORTED BY Z-FURRING

Metal	R-value of	Z-furring			Cavity I	nsulation		
Framing	Foam Board Insulation	Attachment	R-0	R-11	R-13	R-15	R-19	R-21
16" o.c.	R-0 (none)	Horizontal	0.352	0.132	0.124	0.118	0.109	0.106
	R-5	Horizontal	0.155	0.089	0.086	0.083	0.078	0.077
	R-7.5	Horizontal	0.128	0.080	0.077	0.074	0.071	0.069
	R-10	Horizontal	0.110	0.072	0.070	0.068	0.065	0.064
	R-12.5	Horizontal	0.099	0.068	0.065	0.064	0.061	0.060
	R-15	Horizontal	0.091	0.064	0.062	0.060	0.058	0.057
	R-17.5	Horizontal	0.084	0.060	0.058	0.057	0.055	0.054
	R-20	Horizontal	0.078	0.057	0.056	0.054	0.052	0.052
	R-22.5	Horizontal	0.074	0.055	0.054	0.052	0.051	0.050
	R-25	Horizontal	0.071	0.053	0.052	0.051	0.049	0.048
	R-0 (none)	Vertical	0.352	0.132	0.124	0.118	0.109	0.106
	R-5	Vertical	0.165	0.093	0.089	0.086	0.081	0.079
	R-7.5	Vertical	0.142	0.085	0.081	0.079	0.075	0.073
	R-10	Vertical	0.126	0.079	0.076	0.074	0.070	0.069
	R-12.5	Vertical	0.115	0.074	0.072	0.070	0.066	0.065
-	R-15	Vertical	0.107	0.071	0.069	0.067	0.064	0.063
	R-17.5	Vertical	0.100	0.068	0.065	0.064	0.061	0.060
	R-20	Vertical	0.094	0.065	0.063	0.061	0.059	0.058
	R-22.5	Vertical	0.090	0.063	0.061	0.060	0.057	0.056
	R-25	Vertical	0.086	0.061	0.059	0.058	0.056	0.055
24" o.c.	R-0 (none)	Horizontal	0.338	0.116	0.108	0.102	0.094	0.09
	R-5	Horizontal	0.152	0.082	0.078	0.074	0.070	0.068
	R-7.5	Horizontal	0.126	0.074	0.070	0.068	0.064	0.062
	R-10	Horizontal	0.109	0.067	0.065	0.062	0.059	0.058
	R-12.5	Horizontal	0.098	0.063	0.061	0.059	0.056	0.055
	R-15	Horizontal	0.090	0.060	0.058	0.056	0.053	0.052
	R-17.5	Horizontal	0.083	0.057	0.055	0.053	0.051	0.050
	R-20	Horizontal	0.078	0.054	0.052	0.051	0.049	0.048
	R-22.5	Horizontal	0.074	0.052	0.050	0.049	0.047	0.046
	R-25	Horizontal	0.070	0.050	0.049	0.047	0.046	0.045
	R-0 (none)	Vertical	0.338	0.116	0.108	0.102	0.094	0.09
-	R-5	Vertical	0.162	0.084	0.080	0.077	0.072	0.070
-	R-7.5	Vertical	0.140	0.078	0.074	0.071	0.067	0.065
-	R-10	Vertical	0.124	0.073	0.070	0.067	0.063	0.062
	R-12.5	Vertical	0.113	0.069	0.066	0.064	0.061	0.059
-	R-15	Vertical	0.106	0.066	0.063	0.061	0.058	0.057
	R-17.5	Vertical	0.098	0.063	0.061	0.059	0.056	0.055
-	R-20	Vertical	0.093	0.061	0.059	0.057	0.054	0.053
	R-22.5	Vertical	0.089	0.059	0.057	0.055	0.053	0.051
	R-25	Vertical	0.085	0.057	0.055	0.054	0.051	0.050

Values may in Table A105.3.6.1(2) may not interpolated between. The value of the foam board insulation must meet exceed the value listed in the table in order to use the value shown.

	Cav	vity		Insulation	
	Nominal	Actual Depth,	Nominal	ominal Effective R-Va	
	Depth, Inches	Inches	R-Value	16" O.C.	24" O.C.
	Any	Any	R-0.91 (air)	0.79	0.91
Air Cavity					
	4	3-1/2	R-11	5.5	6.6
	4	3-1/2	R-13	6.0	7.2
Wall	4	3-1/2	R-15	6.4	7.8
Wall	6	5-1/2	R-19	7.1	8.6
	6	5-1/2	R-21	7.4	9.0
	8	7-1/4	R-25	7.8	9.6
		In contraction in	R-11	5.5	6.1
Roof		Insulation is uncompressed	R-19	7.0	9.1
		uncompressed	R-30	9.3	11.4

### TABLE A103.3.6.2 EFFECTIVE R-VALUES FOR METAL FRAMING AND CAVITY ONLY

#### TABLE A103.3.6.3 DEFAULT METAL BUILDING WALL U-FACTORS

Insulation	Rated R-	Overall U-fFactor for	Overall U-Factor for Assembly of Base Wall Plus Continuous Insulation (Uninterrupted by Framing)							
System	Value of Insulation	Entire Base Wall Assembly	R-6.5	R-13	R-19.5	R-26	R-32.5	<b>R-39</b> 0.025 0.023		
Single Laye	Single Layer of Mineral Fiber									
	None	1.180	0.136	0.072	0.049	0.037	0.030	0.025		
	R-10	0.186	0.084	0.054	0.040	0.032	0.026	0.023		
	R-11	0.185	0.084	0.054	0.040	0.032	0.026	0.023		
	R-13	0.162	0.079	0.052	0.039	0.031	0.026	0.022		
	R-16	0.155	0.077	0.051	0.039	0.031	0.026	0.022		
	R-19	0.147	0.075	0.050	0.038	0.030	0.025	0.022		

#### TABLE A103.3.7.1(1) DEFAULT U-FACTORS FOR CONCRETE AND MASONRY WALLS

#### 8" Concrete Masonry

WALL DESCRIPTION	CORE TREATMENT				
	Partial Grout with Ungrouted Cores				
	Emphy	Loose-fil	l insulated	Solid Grout	
	Empty	Perlite	Vermiculite	]	
Exposed Block, Both Sides	0.40	0.23	0.24	0.43	
R-5 Interior Insulation, Wood Furring	0.14	0.11	0.12	0.15	
R-6 Interior Insulation, Wood Furring	0.14	0.11	0.11	0.14	
R-10.5 Interior Insulation, Wood Furring	0.11	0.09	0.09	0.11	
R-8 Interior Insulation, Metal Clips	0.11	0.09	0.09	0.11	
R-6 Exterior Insulation	0.12	0.10	0.10	0.12	
R-10 Exterior Insulation	0.08	0.07	0.07	0.08	
R-9.5 Rigid Polystyrene Integral Insulation, Two					
Webbed Block	0.11	0.09	0.09	0.12	

#### 12" Concrete Masonry

WALL DESCRIPTION	CORE TREATMENT				
	Partial Grout with Ungrouted Cores				
	Emerativ	Loose-fi	Il insulated	Solid Grout	
	Empty	Perlite	Vermiculite		
Exposed Block, Both Sides	0.35	0.17	0.18	0.33	
R-5 Interior Insulation, Wood Furring	0.14	0.10	0.10	0.13	
R-6 Interior Insulation, Wood Furring	0.13	0.09	0.10	0.13	
R-10.5 Interior Insulation, Wood Furring	0.11	0.08	0.08	0.10	
R-8 Interior Insulation, Metal Clips	0.10	0.08	0.08	0.09	
R-6 Exterior Insulation	0.11	0.09	0.09	0.11	
R-10 Exterior Insulation	0.08	0.06	0.06	0.08	
R-9.5 Rigid Polystyrene Integral Insulation, Two Webbed Block	0.11	0.08	0.09	0.12	

#### 8" Clay Brick

WALL DESCRIPTION		CORE TREATMENT				
	Partial G	Partial Grout with Ungrouted Cores				
	Emerter	Loose-fi	ll insulated	Solid Grout		
	Empty	Perlite	Vermiculite			
Exposed Block, Both Sides	0.50	0.31	0.32	0.56		
R-5 Interior Insulation, Wood Furring	0.15	0.13	0.13	0.16		
R-6 Interior Insulation, Wood Furring	0.15	0.12	0.12	0.15		
R-10.5 Interior Insulation, Wood Furring	0.12	0.10	0.10	0.12		
R-8 Interior Insulation, Metal Clips	0.11	0.10	0.10	0.11		
R-6 Exterior Insulation	0.12	0.11	0.11	0.13		
R-10 Exterior Insulation	0.08	0.08	0.08	0.09		

#### TABLE A103.3.7.1(1) – continued DEFAULT U-FACTORS FOR CONCRETE AND MASONRY WALLS

#### **6" Concrete Poured or Precast**

WALL DESCRIPTION	CORE TREATMENT				
	Partial G	Partial Grout with Ungrouted Cores			
	Emerativ	Loose-fi	II insulated	Solid Grout	
	Empty	Perlite	Vermiculite		
Exposed Concrete, Both Sides	NA	NA	NA	0.61	
R-5 Interior Insulation, Wood Furring	NA	NA	NA	0.16	
R-6 Interior Insulation, Wood Furring	NA	NA	NA	0.15	
R-10.5 Interior Insulation, Wood Furring	NA	NA	NA	0.12	
R-8 Interior Insulation, Metal Clips	NA	NA	NA	0.12	
R-6 Exterior Insulation	NA	NA	NA	0.13	
R-10 Exterior Insulation	NA	NA	NA	0.09	

1. Grouted cores at 40" x 48" on center vertically and horizontally in partial grouted walls.

2. Interior insulation values include 1/2" gypsum board on the inner surface.

3. Furring and stud spacing is 16" on center. Insulation is assumed to fill furring space and is not compressed.

- 4. Intermediate values may be interpolated using this table. Values not contained in this table may be computed using the procedures listed in the ASHRAE Fundamentals Handbook.
- 5. Concrete Masonry Unit (CMU) assembly U-values are based on local test data for Washington state CMU block material using the ASTM C-236-87 steady state thermal conductance test. Tests included an 8"x8"x16" CMU with all cells filled with vermiculite (1995) and 8"x8"x16" CMU with all cells filled with polymaster foam in place insulation (1996). Refer to ASHRAE Standard 90.1 for additional nationally recognized data on the thermal performance of CMU block walls.

#### TABLE A103.3.7.1(4) DEFAULT U-FACTORS FOR CONCRETE AND MASONRY WALLS

Framing Type and Depth	Rated R-Value of Insulation Alone	Assembly U-Factors for Solid Concrete Walls	Assembly U-Factors for Concrete Block Walls: Solid Grouted	Assembly U-Factors for Concrete Block Walls: Partially Grouted (cores uninsulated except where specified)
Base Wall only				
No Framing	R-0	U-0.740	U-0.580	U-0.480
	Ungrouted Cores Filled with Loose-Fill Insulation	N.A.	N.A.	U-0.350
Continuous Wood F	raming			
0.75 in.	R-3.0	U-0.247	U-0.226	U-0.210
1.5 in.	R-6.0	U-0.160	U-0.151	U-0.143
2.0 in.	R-10.0	U-0.116	U-0.111	U-0.107
3.5 in.	R-11.0	U-0.094	U-0.091	U-0.088
3.5 in.	R-13.0	U-0.085	U-0.083	U-0.080
3.5 in.	R-15.0	U-0.079	U-0.077	U-0.075
5.5 in.	R-19.0	U-0.060	U-0.059	U-0.058
5.5 in.	R-21.0	U-0.057	U-0.055	U-0.054

Framing Type and Depth	Rated R-Value of Insulation Alone	Assembly U-Factors for Solid Concrete Walls	Assembly U-Factors for Concrete Block Walls: Solid Grouted	Assembly U-Factors for Concrete Block Walls: Partially Grouted (cores uninsulated except where specified)
Continuous Metal Fr	aming at 24 in. on center h	orizontally		
1.0 in.	R-0.0	U-0.414	U-0.359	U-0.318
1.0 in.	R-3.8	U-0.325	U-0.290	U-0.263
1.0 in.	R-5.0	U-0.314	U-0.281	U-0.255
1.0 in.	R-6.5	U-0.305	U-0.274	U-0.249
1.5 in.	R-11.0	U-0.267	U-0.243	U-0.223
2.0 in.	R-7.6	U-0.230	U-0.212	U-0.197
2.0 in.	R-10.0	U-0.219	U-0.202	U-0.188
2.0 in.	R-13.0	U-0.210	U-0.195	U-0.182
3.0 in.	R-11.4	U-0.178	U-0.167	U-0.157
3.0 in.	R-15.0	U-0.168	U-0.158	U-0.149
3.0 in.	R-19.0	U-0.161	U-0.152	U-0.144
3.5 in.	R-11.0	U-0.168	U-0.158	U-0.149
3.5 in.	R-13.0	U-0.161	U-0.152	U-0.144
3.5 in.	R-15.0	U-0.155	U-0.147	U-0.140
4.5 in.	R-17.1	U-0.133	U-0.126	U-0.121
4.5 in.	R-22.5	U-0.124	U-0.119	U-0.114
4.5 in.	R-25.2	U-0.122	U-0.116	U-0.112
5.0 in.	R-19.0	U-0.122	U-0.117	U-0.112
5.0 in.	R-25.0	U-0.115	U-0.110	U-0.106
5.0 in.	R-28.0	U-0.112	U-0.107	U-0.103
5.0 in.	R-32.0	U-0.109	U-0.105	U-0.101
5.5 in.	R-19.0	U-0.118	U-0.113	U-0.109
5.5 in.	R-20.9	U-0.114	U-0.109	U-0.105
5.5 in.	<b>R-21.0</b>	U-0.113	U-0.109	U-0.105
5.5 in.	R-27.5	U-0.106	U-0.102	U-0.099
5.5 in.	R-30.8	U-0.104	U-0.100	U-0.096
6.0 in.	R-22.8	U-0.106	U-0.102	U-0.098
6.0 in.	R-30.0	U-0.099	U-0.095	U-0.092
6.0 in.	R-33.6	U-0.096	U-0.093	U-0.090
6.5 in.	R-24.7	U-0.099	U-0.096	U-0.092
7.0 in.	R-26.6	U-0.093	U-0.090	U-0.087
7.5 in.	R-28.5	U-0.088	U-0.085	U-0.083
8.0 in.	R-30.4	U-0.083	U-0.081	U-0.079

#### TABLE A103.3.7.1(4) (Continued) DEFAULT U-FACTORS FOR CONCRETE AND MASONRY WALLS

Framing Type and Depth	Rated R-Value of Insulation Alone	Assembly U-Factors for Solid Concrete Walls	Assembly U-Factors for Concrete Block Walls: Solid Grouted	Assembly U-Factors for Concrete Block Walls: Partially Grouted (cores uninsulated except where specified)
	4 in. on center horizontally by Section C402.1.3, for a		al penetration area/ mass wa	ll area of <0.0004 or <0.04% of
1.0 in.	R-3.8	U-0.210	U-0.195	U-0.182
1.0 in.	R-5.0	U-0.184	U-0.172	U-0.162
1.0 in.	R-5.6	U-0.174	U-0.163	U-0.154
1.5 in.	R-5.7	U-0.160	U-0.151	U-0.143
1.5 in.	R-7.5	U-0.138	U-0.131	U-0.125
1.5 in.	R-8.4	U-0.129	U-0.123	U-0.118
2.0 in.	R-7.6	U-0.129	U-0.123	U-0.118
2.0 in.	R-10.0	U-0.110	U-0.106	U-0.102
2.0 in.	R-11.2	U-0.103	U-0.099	U-0.096
2.5 in.	R-9.5	U-0.109	U-0.104	U-0.101
2.5 in.	R-12.5	U-0.092	U-0.089	U-0.086
2.5 in.	R-14.0	U-0.086	U-0.083	U-0.080
3.0 in.	R-11.4	U-0.094	U-0.090	U-0.088
3.0 in.	R-15.0	U-0.078	U-0.076	U-0.074
3.0 in.	R-16.8	U-0.073	U-0.071	U-0.069
3.5 in.	R-13.3	U-0.082	U-0.080	U-0.077
3.5 in.	R-17.5	U-0.069	U-0.067	U-0.065
3.5 in.	R-19.6	U-0.064	U-0.062	U-0.061
4.0 in.	R-15.2	U-0.073	U-0.071	U-0.070
4.0 in.	R-20.0	U-0.061	U-0.060	U-0.058
4.0 in.	R-22.4	U-0.057	U-0.056	U-0.054
5.0 in.	R-28.0	U-0.046	U-0.046	U-0.045
6.0 in.	R-33.6	U-0.039	U-0.039	U-0.038
7.0 in.	R-39.2	U-0.034	U-0.034	U-0.033
8.0 in.	R-44.8	U-0.030	U-0.030	U-0.029
9.0 in.	R-50.4	U-0.027	U-0.027	U-0.026
10.0 in.	R-56.0	U-0.024	U-0.024	U-0.024
11.0 in.	R-61.6	U-0.022	U-0.022	U-0.022
	on Uninterrupted by Framin			
No Framing	R-1.0	U-0.425	U-0.367	U-0.324
g	R-2.0	U-0.298	U-0.269	U-0.245
	R-3.0	U-0.230	U-0.212	U-0.197
	R-4.0	U-0.187	U-0.175	U-0.164
	R-5.0	U-0.157	U-0.149	U-0.141

#### TABLE A103.3.7.1(4) – continued DEFAULT U-FACTORS FOR CONCRETE AND MASONRY WALLS

Framing Type and Depth	Rated R-Value of Insulation Alone	Assembly U-Factors for Solid Concrete Walls	Assembly U-Factors for Concrete Block Walls: Solid Grouted	Assembly U-Factors for Concrete Block Walls: Partially Grouted (cores uninsulated except where specified)
No Framing	R-6.0	U-0.136	U-0.129	U-0.124
	R-7.0	U-0.120	U-0.115	U-0.110
	R-8.0	U-0.107	U-0.103	U-0.099
	R-9.0	U-0.097	U-0.093	U-0.090
	R-10.0	U-0.088	U-0.085	U-0.083
No Framing	R-11.0	U-0.081	U-0.079	U-0.076
	R-12.0	U-0.075	U-0.073	U-0.071
	R-13.0	U-0.070	U-0.068	U-0.066
	R-14.0	U-0.065	U-0.064	U-0.062
	R-15.0	U-0.061	U-0.060	U-0.059
No Framing	R-16.0	U-0.058	U-0.056	U-0.055
	R-17.0	U-0.054	U-0.053	U-0.052
	R-18.0	U-0.052	U-0.051	U-0.050
	R-19.0	U-0.049	U-0.048	U-0.047
	R-20.0	U-0.047	U-0.046	U-0.045
No Framing	R-21.0	U-0.045	U-0.044	U-0.043
	R-22.0	U-0.043	U-0.042	U-0.042
	R-3.0	U-0.041	U-0.040	U-0.040
	R-24.0	U-0.039	U-0.039	U-0.038
	R-25.0	U-0.038	U-0.037	U-0.037
No Framing	R-30.0	U-0.032	U-0.032	U-0.031
	R-35.0	U-0.028	U-0.027	U-0.027
	R-40.0	U-0.024	U-0.024	U-0.024
	R-45.0	U-0.022	U-0.021	U-0.021
	R-50.0	U-0.019	U-0.019	U-0.019
	R-55.0	U-0.018	U-0.018	U-0.018
	R-60.0	U-0.016	U-0.016	U-0.016
Brick cavity wall v	with continuous insula	tion		
No Framing	R-0.0	U-0.337	U-0.299	U-0.270
No Framing	R-3.8	U-0.148	U-0.140	U-0.133
No Framing	R-5.0	U-0.125	U-0.120	U-0.115
No Framing	R-6.5	U-0.106	U-0.102	U-0.098
No Framing	R-7.6	U-0.095	U-0.091	U-0.088
No Framing	R-10.0	U-0.077	U-0.075	U-0.073
No Framing	R-10.5	U-0.079	U-0.077	U-0.075
No Framing	R-11.4	U-0.070	U-0.068	U-0.066
No Framing	R-15.0	U-0.056	U-0.055	U-0.053
No Framing	R-16.5	U-0.054	U-0.053	U-0.052
No Framing	R-19.0	U-0.046	U-0.045	U-0.044
No Framing		U-0.040	U-0.040	U-0.039
5	R-22.5			
No Framing	R-28.5	U-0.033	U-0.032	U-0.032

#### TABLE A103.3.7.1(2) – continued DEFAULT U-FACTORS FOR CONCRETE AND MASONRY WALLS

Framing Type and Depth	Rated R-Value of Insulation Alone	Assembly U-Factors for Solid Concrete Walls	Assembly U-Factors for Concrete Block Walls: Solid Grouted	Assembly U-Factors for Concrete Block Walls: Partially Grouted (cores uninsulated except where specified)
Continuous Insulation	on Uninterrupted by Framing	g with Stucco and Continuou	s Metal Framing at 24 in. on	center horizontally
1.0 in.	R-0.0 + R-19 c.i.	U-0.047	U-0.046	U-0.045
1.0 in.	R-3.8 + R-19 c.i.	U-0.045	U-0.044	U-0.044
1.0 in.	R-5.0 + R-19 c.i.	U-0.045	U-0.044	U-0.043
1.0 in.	R-6.5 + R-19 c.i.	U-0.045	U-0.044	U-0.043
1.5 in.	R-11.0 + R-19 c.i.	U-0.044	U-0.043	U-0.043
2.0 in.	R-7.6 + R-19 c.i.	U-0.043	U-0.042	U-0.041
2.0 in.	R-10.0 + R-19 c.i.	U-0.042	U-0.041	U-0.041
2.0 in.	R-13.0 + R-19 c.i.	U-0.042	U-0.041	U-0.041
3.0 in.	R-11.4 + R-19 c.i.	U-0.041	U-0.040	U-0.039
3.0 in.	R-15.0 + R-19 c.i.	U-0.040	U-0.039	U-0.039
3.0 in.	R-19.0 + R-19 c.i.	U-0.040	U-0.039	U-0.038
3.5 in.	R-11.0 + R-19 c.i.	U-0.040	U-0.039	U-0.039
3.5 in.	R-13.0 + R-19 c.i.	U-0.040	U-0.039	U-0.038
5.0 in.	R-19.0 + R-19 c.i.	U-0.037	U-0.036	U-0.036
5.0 in.	R-25.0 + R-19 c.i.	U-0.036	U-0.035	U-0.035
5.0 in.	R-32.5 + R-19 c.i.	U-0.035	U-0.035	U-0.034
5.5 in.	R-19.0 + R-19 c.i.	U-0.036	U-0.036	U-0.035
5.5 in.	R-21.0 + R-19 c.i.	U-0.035	U-0.035	U-0.035

#### TABLE A103.3.7.1(2) – continued DEFAULT U-FACTORS FOR CONCRETE AND MASONRY WALLS

#### Notes for Default Table A103.3.7.1(4):

- a. It is acceptable to use the U-factors in Table A103.3.7.1(4) for all concrete and masonry walls, provided that the grouting is equal to or less than that specified.
  - -For ungrouted walls, use the partially grouted column.
  - -For metal studs and z-furring, use the continuous-metal-framing category.
  - -For discontinuous metal clips 1 inch square or smaller, use the metal-clip category.
  - -For insulation that is attached without any framing members (e.g. glued), use the continuous-insulation uninterrupted-by-framing category. Continuous insulation may be installed on the interior or exterior of masonry walls, or between stand-alone walls in multilayer masonry walls, or on the interior or exterior of the concrete.
- b. For Table A103.3.7.1(4), the U-factor includes R-0.17 for exterior air film and R-0.68 for interior air film-vertical surfaces. For insulated walls, the U-factor also includes R-0.45 for 0.5 in. gypsum board. U-factors are provided for the following configurations:
  - 1. Concrete wall: 8-in. normal weight concrete wall with a density of 145 lb/ft<sup>3</sup>.
  - 2. Solid grouted concrete block wall: 8-in. medium weight ASTM C90 concrete block with a density of 115 lb/ft<sup>3</sup> and solid grouted cores.
  - 3. Partially grouted concrete block wall: 8-in. medium weight ASTM C90 concrete block with a density of 115 lb/ft<sup>3</sup> having reinforcing steel every 32 in. vertically and every 48 in. horizontally, with cores grouted in those areas only. Other cores are filled with insulating material only if there is no other insulation.
- c. For walls with insulation contained in a framing layer, the U-factors in Table A103.3.7.1(4) assume contact (and thermal bridging) between the mass wall and other framing. For wall assemblies with multiple layers where the wood or metal framing layer does not contact the concrete or masonry layer (i.e., walls with an airspace between the stud wall layer and the mass wall layer), it is acceptable to use the appropriate wood or metal frame wall default U-factors in Tables A103.3.1 or A103.3.6.1. Note: It is acceptable to use this approach where the insulation extends beyond the framing and is in contact with the mass wall layer (e.g. a nominal four-inch metal stud containing insulation that is nominally six inches thick and therefore extends two inches beyond the back of the metal stud).
- d. Except for wall assemblies qualifying for note 3, if not taken from Table A103.3.7.1(2), mass wall U-factors shall be determined in accordance with ASHRAE 90.1, Appendix A, Section A3.1 and Tables A3.1A to A3.1D, or Section A9.4.

Slab Edge Treatment	Average Thickness of Wall Above and Below				
	6 inches	8 inches	10 inches	12 inches	
Exposed Concrete	0.816	0.741	0.678	0.625	
<b>R-5</b> Exterior Insulation	0.161	0.157	0.154	0.152	
<b>R-6</b> Exterior Insulation	0.138	0.136	0.134	0.132	
<b>R-7</b> Exterior Insulation	0.122	0.120	0.118	0.116	
<b>R-8</b> Exterior Insulation	0.108	0.107	0.106	0.104	
<b>R-9</b> Exterior Insulation	0.098	0.097	0.095	0.094	
<b>R-10</b> Exterior Insulation	0.089	0.088	0.087	0.086	
R-11 Exterior Insulation	0.082	0.081	0.080	0.079	
R-12 Exterior Insulation	0.076	0.075	0.074	0.074	
R-13 Exterior Insulation	0.070	0.070	0.069	0.068	
R-14 Exterior Insulation	0.066	0.065	0.065	0.064	
R-15 Exterior Insulation	0.062	0.061	0.061	0.060	

### TABLE A103.3.7.2DEFAULT U-FACTORS FORPERIPHERAL EDGES OF INTERMEDIATE CONCRETE FLOORS

Notes for Table A103.3.7.2:

a. Exterior insulation values listed above are continuous R-values on the exterior side of the concrete floor.

b. For conditions with an exterior wall above the peripheral edge of intermediate concrete floor but with no wall below the intermediate concrete floor this table may be used as long as the code minimum insulation is applied to the floor slab below the concrete floor.

c. Typical conditions where conditioned space building envelope wall thermal insulation values are broken concrete floors include, but are not limited to, the following examples:

- 1. Elevator hoistway shafts that serve the conditioned building and pass through unconditioned floors such as parking garage levels;
- 2. Stairwell enclosures that serve the conditioned building and pass through unconditioned floors such as parking garage levels;
- 3. Walls between interior and exterior building envelope that separate the interior conditioned space from an exterior courtyard or roofdeck;
- 4. Walls between interior and exterior building envelope that separate the interior conditioned space from an exterior unconditioned space on parking garage levels.

#### SECTION A104 BELOW-GRADE WALLS AND SLABS

**A104.1 General.** Table A104.1 lists heat loss coefficients for below-grade walls and floors.

Coefficients for below-grade walls are given as U-factors (Btu/h  $\times$  ft<sup>2</sup>  $\times$  °F of wall area). Coefficients for below-grade slabs are listed as F-factors (Btu/h  $\times$  ft  $\times$  °F per lineal foot of slab perimeter).

Below-grade wall U-factors are only valid when used with the accompanying below-grade slab F-factor, and vice versa.

**A104.2 Component description.** All below-grade walls are assumed to be 8 inch concrete. The wall is assumed to extend from the slab upward to the top of the mud sill for the distance specified in Table A104.1, with 6 inches of concrete wall extending above grade.

Interior insulation is assumed to be fiberglass batts placed in the cavity formed by 2 x 4 framing on 24 inch centers with 1/2 inch gypsum board as the interior finish material. Exterior insulation is assumed to be applied directly to the exterior of the below-grade wall from the top of the wall to the footing. The exterior case does not assume any interior framing or sheetrock.

In all cases, the entire wall surface is assumed to be insulated to the indicated nominal level with the appropriate framing and insulation application. Coefficients are listed for wall depths of 2, 3-1/2 and 7 feet below grade. Basements shallower than two feet should use on-grade slab coefficients.

Heat-loss calculations for wall areas above-grade should use above-grade wall U-factors, beginning at the mudsill.

	Below Grade Wall U-factor	Below Grade Slab F-factor
2 Foot Depth Below Grade		
Uninsulated	0.350	0.59
R-11 Interior	0.066	0.68
R-11 Interior w/TB	0.070	0.60
R-19 Interior	0.043	0.69
R-19 Interior w/TB	0.045	0.61
R-10 Exterior	0.070	0.60
R-12 Exterior	0.061	0.60
3.5 Foot Depth Below Grad	le	
Uninsulated	0.278	0.53
R-11 Interior	0.062	0.63
R-11 Interior w/TB	0.064	0.57
R-19 Interior	0.041	0.64
R-19 Interior w/TB	0.042	0.57
R-10 Exterior	0.064	0.57
R-12 Exterior	0.057	0.57
7 Foot Depth Below Grade		
Uninsulated	0.193	0.46
R-11 Interior	0.054	0.56
R-11 Interior w/TB	0.056	0.42
R-19 Interior	0.037	0.57
R-19 Interior w/TB	0.038	0.43
R-10 Exterior	0.056	0.42
R-12 Exterior	0.050	0.42

TABLE A104.1
DEFAULT WALL U-FACTORS AND SLAB F-FACTORS FOR BASEMENTS

TB = Thermal Break

**A104.3 Insulation description.** Coefficients are listed for the following four configurations:

- 1. Uninsulated: No insulation or interior finish.
- 2. **Interior insulation:** Interior 2 x 4 insulated wall without a thermal break between concrete wall and slab.
- 3. **Interior insulation with thermal break:** Interior 2 x 4 insulated wall with R-5 rigid board providing a thermal break between the concrete wall and the slab.
- 4. **Exterior insulation:** Insulation applied directly to the exterior surface of the concrete wall.

#### SECTION A105 FLOORS OVER UNCONDITIONED SPACE

**A105.1 General.** Tables A105.1(1), A105.1(2) and A105.1(3) list heat loss coefficients for floors over unconditioned spaces in units of Btu/h  $\times$  ft<sup>2</sup>  $\times$  °F.

They are derived from procedures listed in the ASHRAE Fundamentals Handbook, assuming an average outdoor temperature of  $45^{\circ}$ F, an average indoor temperature of  $65^{\circ}$ F and a crawlspace area of 1350 ft<sup>2</sup> and 100 feet of perimeter. The crawlspace is assumed to be 2.5 feet high, with 24 inches below grade and 6 inches above grade.

#### TABLE A105.1(1) DEFAULT U-FACTORS FOR WOOD-FRAMED FLOORS OVER VENTED CRAWLSPACE OR UNHEATED BASEMENT

Nominal R-Value		U-Fa	octor
Floor	Perimeter	Post & Beam	Joists
0	0	0.112	0.134
	11	0.100	0.116
	19	0.098	0.114
	30	0.093	0.107
11	0	0.052	0.056
	11	0.048	0.052
19	0	0.038	0.041
	11	0.036	0.038
22	0	0.034	0.037
	11	0.033	0.035
25	0	0.032	0.034
	11	0.031	0.033
30	0	0.028	0.029
	11	0.027	0.028
38	0	0.024	0.025
	11	0.024	0.024

#### TABLE A105.1(2) DEFAULT U-FACTORS FOR WOOD-FRAMED FLOORS OVER HEATED PLENUM CRAWLSPACES

Nominal R-Value Perimeter	U-Factor
11	0.085
19	0.075
30	0.069

**Note:** Crawlspaces used as heated plenums have approximately 30% higher heat loss rate than unvented crawlspaces with the same assumed ACH. Default U-factors in Table A105.1(2) reflect this higher rate of heat loss.

U-Factor				
Nominal R-Value	Concrete	Wood Joist	Metal Joist	
R-11	0.077	0.088	0.14	
R-15	0.059	0.076	0.12	
R-19	0.048	0.062	0.11	
R-21	0.043	0.057	0.11	
R-25	0.037	0.051	0.10	
R-30	0.031	0.040	0.09	
R-38	0.025	0.034	0.08	

#### TABLE A105.1(3) DEFAULT U-FACTORS FOR EXPOSED FLOORS

#### A105.2 Crawlspace description. Four

configurations are considered: Naturally ventilated crawlspace, mechanically vented crawlspace, heated plenum crawlspace and exposed floor.

#### A105.2.1 Naturally ventilated crawlspaces.

Assumed to have 3.0 air changes per hour, with at least 1.0  $\text{ft}^2$  of net-free ventilation in the foundation for every 300  $\text{ft}^2$  of crawlspace floor area. The crawlspace is not actively heated. Floors over unheated areas, such as garages, may only use those values which have R-0 perimeter insulation.

#### A105.2.2 Mechanically ventilated crawlspaces.

Assume to have 1.5 air changes per hour, with less than 1.0  $\text{ft}^2$  of net-free ventilation in the foundation for every 300  $\text{ft}^2$  of crawlspace floor area. The crawlspace is not actively heated. Floors over unheated basements may only use those values which have R-0 perimeter insulation.

**A105.2.3 Heated plenum crawlspaces.** Assumed to have 0.25 air changes per hour, with no foundation vents. Heated supply air from central furnace is blown into a crawlspace and allowed to enter the living space unducted via holes cut into the floor.

A105.2.4 Exposed floors. Assumes no buffer space, and a covering of 1/2 inch T1-11 on the exterior of

the cavity exposed to the outside air or rigid insulation below a concrete floor, such as over parking garages.

**A105.3 Construction description.** Floors are assumed to be either joisted floors framed on 16 inch centers, or post and beam on 4 foot by 8 foot squares. Insulation is assumed to be installed under the subflooring between the joists or beams with no space between the insulation and the subfloor. Insulation is assumed to be uncompressed. Exposed floors also include concrete with continuous rigid insulation assumed.

Perimeter insulation is assumed to extend from the top of the rim joist to the crawlspace floor and then inward along the ground (on top of the ground cover) for at least 24 inches.

Floor coverings are assumed to be light carpet with rubber pad.

#### SECTION A106 ON-GRADE SLAB FLOORS

**A106.1 General.** Table A106.1 lists heat loss coefficients for heated on-grade slab floors, in units of  $Btu/h \times {}^{\circ}F$  per lineal foot of perimeter.

Insulation type	R-0	R-5	R-10	R-15
		Unhea	ated Slab	
Uninsulated slab	0.73			
2 ft Horizontal (No thermal break)		0.70	0.70	0.69
4 ft Horizontal (No thermal break)		0.67	0.64	0.63
2 ft Vertical		0.58	0.54	0.52
4 ft Vertical		0.54	0.48	0.45
Fully insulated slab			0.36	
		Hea	ted Slab	
Uninsulated slab	0.84			
Fully insulated slab		0.74	0.55	0.44
R-5 Center (With perimeter insulation)			0.66	0.62
R-10 Center (With perimeter insulation)				0.51
3 ft Vertical			0.78	

#### TABLE A106.1 DEFAULT F-FACTORS FOR ON-GRADE SLABS

**A106.2 Component description.** All on-grade slab floors are assumed to be 6 inch concrete poured directly onto the earth. The bottom of the slab is assumed to be at grade line. Monolithic and floating slabs are not differentiated.

Soil is assumed to have a conductivity of 0.75 Btu/h  $\times$  ft<sup>2</sup>  $\times$  °F. Slabs 2 feet or more below grade should use basement coefficients.

**A106.3 Insulation description.** Coefficients are provided for the following three configurations:

- 1. **Two foot (or four foot) vertical:** Insulation is applied directly to the slab exterior, extending downward from the top of the slab to a depth of 2 feet (or 4 feet) below grade.
- 2. **Two foot (or four foot) horizontal:** Insulation is applied directly to the underside of the slab, and run horizontally from the perimeter inward for 2 feet (or 4 feet). The slab edge is exposed in this configuration.

- **Note:** A horizontal installation with a thermal break of at least R-5 at the slab edge should use the vertical-case F-factors.
- 3. **Fully insulated slab:** Insulation extends from the top of the slab, along the entire perimeter, and completely covers the area under the slab. Thicker perimeter insulation covers the slab edge and extends 2 feet under the slab.

#### SECTION A107 DEFAULT U-FACTORS FOR DOORS

**A107.1 Doors without NFRC certification.** Doors that do not have NFRC certification shall be assigned the appropriate U-factor from Tables A107.1(1) through A107.1(4).

#### TABLE A107.1(1) DEFAULT U-FACTORS FOR DOORS

Door Type	No Glazed Fenestration	Single Glazing	Double Glazing with ¼ in. Airspace	Double Glazing with ½ in. Airspace	Double Glazing with e=0.10, ½ in. Argon
SWINGING DO	OORS (Rough ope	ening – 38 i	n. x 82 in.)		
Slab Doors		1		-	
Wood slab in wood frame <sup>a</sup>	0.46				
6% glazed fenestration (22 in. x 8 in. lite)	_	0.48	0.47	0.46	0.44
25% glazed fenestration (22 in.x36 in. lite)	_	0.58	0.48	0.46	0.42
45% glazed fenestration (22 in.x64 in. lite)	-	0.69	0.49	0.46	0.39
More than 50% glazed fenestration	Use Ta	able C303.1.	3(1)/R303.1.3(	1) as appropri	iate
Insulated steel slab with wood edge in wood frame <sup>a</sup>	0.16				
6% glazed fenestration (22 in. x 8 in. lite)	_	0.21	0.20	0.19	0.18
25% glazed fenestration (22 in.x36 in. lite)	-	0.39	0.28	0.26	0.23
45% glazed fenestration (22 in.x64 in. lite)	_	0.58	0.38	0.35	0.26
More than 50% g glazed fenestration	Use Table C303.1.3(1)/R303.1.3(1) as appropriate				
Foam insulated steel slab with metal edge in steel frame <sup>b</sup>	0.37				
6% glazed fenestration (22 in. x 8 in. lite)	-	0.44	0.42	0.41	0.39
25% glazed fenestration (22 in.x36 in. lite)	_	0.55	0.50	0.48	0.44
45% glazed fenestration (22 in.x64 in. lite)	—	0.71	0.59	0.56	0.48
More than 50% glazed fenestration	Use Table C303.1.3(1)/R303.1.3(1) as appropriate				iate
Cardboard honeycomb slab with metal edge in steel frame <sup>b</sup>	0.61				
Style and Rail Doors					
Sliding glass doors/French doors	Use Ta	able C303.1.	3(1)/R303.1.3(	1) as appropri	iate
Site-Assembled Style and Rail Doors	Site-Assembled Style and Rail Doors				
Aluminum in aluminum frame	_	1.32	0.99	0.93	0.79
Aluminum in aluminum frame with thermal break	-	1.13	0.80	0.74	0.63

a. Thermally broken sill (add 0.03 for non-thermally broken sill)

b. Non-thermally broken sill

c. Nominal U-factors are through the center of the insulated panel before consideration of thermal bridges around the edges of the door section and due to the frame.

<b>Revolving Doors</b>		
Size (W x H)	U-Factor	
3-wing		
8 ft x 7 ft	0.79	
10 ft x 8 ft	0.80	
4-wing		
7 ft x 6.5 ft	0.63	
7 ft x 7.5 ft	0.64	
Open		
82 in x 84 in	1.32	

# TABLE A107.1(2)DEFAULT U-FACTORS FOR REVOLVING DOORS

## TABLE A107.1(3) DEFAULT U-FACTORS FOR STEEL EMERGENCY DOORS

Double-Skin Steel Emergency Exit Doors			
Core Insulation3 ft x 6 ft 8 in6 ft x 6 ft 8			
1-3/8 in. thickness			
Honeycomb kraft paper	0.57	0.52	
Mineral wool, steel ribs	0.44	0.36	
Polyurethane foam	0.34	0.28	
1-3/4 in. thickness			
Honeycomb kraft paper	0.57	0.54	
Mineral wool, steel ribs	0.41	0.33	
Polyurethane foam	0.31	0.26	
1-3/8 in. thickness			
Honeycomb kraft paper	0.60	0.55	
Mineral wool, steel ribs	0.47	0.39	
Polyurethane foam	0.37	0.31	
1-3/4 in. thickness			
Honeycomb kraft paper	0.60	0.57	
Mineral wool, steel ribs	0.44	0.37	
Polyurethane foam	0.34	0.30	

Double-Skin Steel Garage and Aircraft Hangar Doors					
Insulation <sup>e</sup>	One-piece tilt-up <sup>a</sup>		Sectional tilt- up <sup>b</sup>	Aircraft hangar	
	8 ft. x 7 ft.	16 ft. x 7 ft.	9 ft. x 7 ft.	72 ft. x 12 ft. <sup>c</sup>	240 ft. x 50 ft. <sup>d</sup>
1-3/8 in. thickness EPS, steel ribs XPS, steel ribs	0.36 0.33	0.33 0.31	0.34-0.39 0.31-0.36		
2 in. thickness EPS, steel ribs XPS, steel ribs	0.31 0.29	0.28 0.26	0.29-0.33 0.27-0.31		
3 in. thickness EPS, steel ribs XPS, steel ribs	0.26 0.24	0.23 0.21	0.25-0.28 0.24-0.27		
4 in. thickness EPS, steel ribs XPS, steel ribs	0.23 0.21	0.20 0.19	0.23-0.25 0.21-0.24		
6 in. thickness EPS, steel ribs XPS, steel ribs	0.20 0.19	0.16 0.15	0.20-0.21 0.19-0.21		
4 in. thickness Non-insulated Expanded polystyrene Mineral wool, steel ribs Extruded polystyrene				1.10 0.25 0.25 0.23	1.23 0.16 0.16 0.15
6 in. thickness Non-insulated Expanded polystyrene Mineral wool, steel ribs Extruded polystyrene				1.10 0.21 0.23 0.20	1.23 0.13 0.13 0.12
Uninsulated All products	1.15				

### TABLE A107.1(4)DEFAULT U-FACTORS FOR STEEL GARAGE AND HANGAR DOORS

a. Values are for thermally broken or thermally unbroken doors.

b. Lower values are for thermally broken doors; upper values are for doors with no thermal break.

c. Typical size for a small private airplane (single-engine or twin).

d. Typical hangar door for a midsize commercial jet airliner.

e. EPS is extruded polystyrene, XPS is expanded polystyrene.

#### SECTION A108 AIR INFILTRATION

**A108.1 General.** Tables A108.1(1) and A108.1(2) list effective air change rates and heat capacities for heat loss due to infiltration for Single-Family Residential.

The estimated seasonal average infiltration rate in air changes per hour (ACH) is given for standard airleakage control (see Section R402.4 for air leakage requirements for Single-Family Residential). The effective air change rate shall be used in calculations for compliance under either the Component Performance or Systems Analysis approaches.

Heat loss due to infiltration shall be computed using the following equation:

 $Q_{infil} = ACH_{eff} * HCP$ 

Where:

 $Q_{infil}$  = Heat loss due to air infiltration.

ACH<sub>eff</sub> = The effective air infiltration rate in Table A108.1(1)

HCP = The Heat Capacity Density Product for the appropriate elevation or climate zone as given below.

#### TABLE A108.1(1) ASSUMED EFFECTIVE AIR CHANGES PER HOUR

Air-Leakage	Air Changes per Hour		
Control Package	Natural	Effective	
Standard	0.35	0.35	

#### TABLE A108.1(2) DEFAULT HEAT CAPACITY/DENSITY PRODUCT FOR AIR

Zone	Average Elevation	Heat Capacity/ Density
1	Mean Sea Level	0.0180 Btu/h•°F
2	2000	0.0168 Btu/h•°F
3	3000	0.0162 Btu/h•°F

#### **Appendix B**

#### DEFAULT INTERNAL LOAD VALUES AND SCHEDULES

#### SECTION B101 GENERAL

B101.1 Scope. The following default internal load values and schedules shall apply to Section C407.

#### SECTION B102 DEFAULT TABLES OF INTERNAL LOADS

**B102 Default tables of internal loads.** Default occupancy densities, receptacle power densities and service hot water consumption are included in Table B102.

TABLE B102				
ACCEPTABLE OCCUPANCY DENSITIES, RECEPTACLE POWER DENSITIES				
AND SERVICE HOT WATER CONSUMPTION <sup>a</sup>				

Building Type	Occupancy Density <sup>b</sup> ft <sup>2</sup> /Person (Btu/h- ft <sup>2</sup> )	Receptacle Power Density <sup>c</sup> , Watts/ ft <sup>2</sup> (Btu/h· ft <sup>2</sup> )	Service Hot Water Quantities <sup>d</sup> Btu/h per person
Assembly	50 (4.60)	0.25 (0.85)	215
Health/Institutional	200 (1.15)	1.00 (3.41)	135
Hotel/Motel	250 (0.92)	0.25 (0.85)	1,110
Light Manufacturing	750 (0.31)	0.20 (0.68)	225
Office	275 (0.84)	0.75 (2.56)	175
Parking Garage	NA	NA	NA
Restaurant	100 (2.30)	0.10 )0.34)	390
Retail	300 (0.77)	0.25 (0.85)	135
School	75 (3.07)	0.50 (1.71)	215
Warehouse	15,000 (0.02)	0.10 (0.34)	225

a. The occupancy densities, receptacle power densities, and service hot water consumption values are from ASHRAE Standard 90.1-1989 and addenda.

b. Values are in square feet of conditioned floor area per person. Heat generation in Btu per person per hour is 230 sensible and 190 latent. Figures in parenthesis are equivalent Btu per hour per square foot.

c. Values are in Watts per square foot of conditioned floor area. Figures in parenthesis are equivalent Btu per hour per square foot. These values are the minimum acceptable. If other process loads are not input (such as for computers, cooking, refrigeration, etc.), it is recommended that receptacle power densities be increased until total process energy consumption is equivalent to 25% of the total.

d. Values are in Btu per person per hour.

#### SECTION B103 DEFAULT SCHEDULES

**B103 Default schedules.** Default schedules for occupancy, lighting, receptacles, HVAC, service hot water, and elevators are included in Tables B103(1) through B103(10).

Hour of Day	0	hedule ccupan ercent	су	Lightir	hedule ng Rece ercent	ptacle		hedule AC Syst	-	Servi	hedule ce Hot V ercent	Water	1	hedule Elevat ercer	or
(Time)		imum L		Max	imum L	oad		-		Мах	kimum L	oad	Max	imum	Load
	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun
1 (12-1 am)	0	0	0	5	5	5	Off	Off	Off	0	0	0	0	0	0
2 (1-2 am)	0	0	0	5	5	5	Off	Off	Off	0	0	0	0	0	0
3 (2-3 am)	0	0	0	5	5	5	Off	Off	Off	0	0	0	0	0	0
4 (3-4 am)	0	0	0	5	5	5	Off	Off	Off	0	0	0	0	0	0
5 (4-5 am)	0	0	0	5	5	5	Off	Off	Off	0	0	0	0	0	0
6 (5-6 am)	0	0	0	5	5	5	On	Off	Off	0	0	0	0	0	0
7 (6-7 am)	0	0	0	40	5	5	On	On	On	0	0	0	0	0	0
8 (7-8 am)	0	0	0	40	30	30	On	On	On	0	0	0	0	0	0
9 (8-9 am)	20	20	10	40	30	30	On	On	On	0	0	0	0	0	0
10 (9-10 am)	20	20	10	75	50	30	On	On	On	5	5	5	0	0	0
11 (10-11 am)	20	20	10	75	50	30	On	On	On	5	5	5	0	0	0
12 (11-12 pm)	80	60	10	75	50	30	On	On	On	35	20	10	0	0	0
13 (12-1 pm)	80	60	10	75	50	65	On	On	On	5	0	0	0	0	0
14 (1-2 pm)	80	60	70	75	50	65	On	On	On	5	0	0	0	0	0
15 (2-3 pm)	80	60	70	75	50	65	On	On	On	5	0	0	0	0	0
16 (3-4 pm)	80	60	70	75	50	65	On	On	On	5	0	0	0	0	0
17 (4-5 pm)	80	60	70	75	50	65	On	On	On	5	0	0	0	0	0
18 (5-6 pm)	80	60	70	75	50	65	On	On	On	0	0	0	0	0	0
19 (6-7 pm)	20	60	70	75	50	65	On	On	On	0	0	0	0	0	0
20 (7-8 pm)	20	60	70	75	50	65	On	On	On	0	65	65	0	0	0
21 (8-9 pm)	20	60	70	75	50	65	On	On	On	0	30	30	0	0	0
22 (9-10 pm)	20	80	70	75	50	65	On	On	On	0	0	0	0	0	0
23 (10-11 pm)	10	10	20	25	50	5	On	On	On	0	0	0	0	0	0
24 (11-12 am)	0	0	0	5	5	5	Off	Off	Off	0	0	0	0	0	0
Total/Day	710	750	700	1155	800	845	1800	1700	1700	70	125	115	0	0	0
Total/Week		50.5	0 hours		74.2	0 hours		124	4 hours		5.	9 hours			0 hours
Total/Year		263	3 hours		386	9 hours		646	5 hours		30	8 hours			0 hours

# TABLE B103(1) ASSEMBLY OCCUPANCY<sup>a</sup>

Wk = Weekday

#### TABLE B103(2) HEALTH OCCUPANCY<sup>a</sup>

Hour of Day (Time)	Oc Po	hedule ccupanc ercent imum L	cy of	Lightin Po	hedule ng Rece ercent imum L	ptacle of		hedule AC Syst	-	Servi P	hedule ice Hot ercent cimum L	Water t Of	P	hedule Elevato <b>ercent</b> imum L	r t <b>o</b> f
	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun
1 (12-1 am)	0	0	0	10	10	5	On	On	On	1	1	1	0	0	0
2 (1-2 am)	0	0	0	10	10	5	On	On	On	1	1	1	0	0	0
3 (2-3 am)	0	0	0	10	10	5	On	On	On	1	1	1	0	0	0
4 (3-4 am)	0	0	0	10	10	5	On	On	On	1	1	1	0	0	0
5 (4-5 am)	0	0	0	10	10	5	On	On	On	1	1	1	0	0	0
6 (5-6 am)	0	0	0	10	10	5	On	On	On	1	1	1	0	0	0
7 (6-7 am)	0	0	0	10	10	5	On	On	On	1	1	1	0	0	0
8 (7-8 am)	10	10	0	50	20	5	On	On	On	17	1	1	2	2	0
9 (8-9 am)	50	30	5	90	40	10	On	On	On	58	20	1	75	46	2
10 (9-10 am)	80	40	5	90	40	10	On	On	On	66	28	1	100	70	2
11 (10-11 am)	80	40	5	90	40	10	On	On	On	78	30	1	100	70	2
12 (11-12 pm)	80	40	5	90	40	10	On	On	On	82	30	1	100	70	2
13 (12-1 pm)	80	40	5	90	40	10	On	On	On	71	24	1	75	51	2
14 (1-2 pm)	80	40	5	90	40	10	On	On	On	82	24	1	100	51	2
15 (2-3 pm)	80	40	5	90	40	10	On	On	On	78	23	1	100	51	2
16 (3-4 pm)	80	40	5	90	40	10	On	On	On	74	23	1	100	51	2
17 (4-5 pm)	80	40	0	30	40	5	On	On	On	63	23	1	100	51	0
18 (5-6 pm)	50	10	0	30	40	5	On	On	On	41	10	1	100	25	0
19 (6-7 pm)	30	10	0	30	10	5	On	On	On	18	1	1	52	2	0
20 (7-8 pm)	30	0	0	30	10	5	On	On	On	18	1	1	52	0	0
21 (8-9 pm)	20	0	0	30	10	5	On	On	On	18	1	1	52	0	0
22 (9-10 pm)	20	0	0	30	10	5	On	On	On	10	1	1	28	0	0
23 (10-11 pm)	0	0	0	30	10	5	On	On	On	1	1	1	0	0	0
24 (11-12 am)	0	0	0	10	10	5	On	On	On	1	1	1	0	0	0
Total/Day	850	380	40	1060	550	160	2400	2400	2400	783	249	24	1136	540	16
Total/Week		46.70	0 hours		60.1	0 hours		16	8 hours		41.8	8 hours		62.3	6 hours
Total/Year	1	243	5 hours		313	4 hours		876	0 hours		214	8 hours		325	1 hours

Wk = Weekday

## TABLE B103(3) HOTEL/MOTEL OCCUPANCY<sup>a</sup>

Hour of Day (Time)	O P	hedule i ccupano ercent imum L	cy of	Lightii P	hedule ng Rece <b>ercent</b> timum L	ptacle of		hedule AC Syst	-	Servi P	hedule ce Hot V ercent timum L	Water t Of	P	hedule Elevato ercent timum L	r t of
	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun
1 (12-1 am)	90	90	70	20	20	30	On	On	On	20	20	25	40	44	55
2 (1-2 am)	90	90	70	15	20	30	On	On	On	15	15	20	33	35	55
3 (2-3 am)	90	90	70	10	10	20	On	On	On	15	15	20	33	35	43
4 (3-4 am)	90	90	70	10	10	20	On	On	On	15	15	20	33	35	43
5 (4-5 am)	90	90	70	10	10	20	On	On	On	20	20	20	33	35	43
6 (5-6 am)	90	90	70	20	10	20	On	On	On	25	25	30	33	35	43
7 (6-7 am)	70	70	70	40	30	30	On	On	On	50	40	50	42	40	52
8 (7-8 am)	40	50	70	50	30	40	On	On	On	60	50	50	42	32	52
9 (8-9 am)	40	50	50	40	40	40	On	On	On	55	50	50	52	45	65
10 (9-10 am)	20	30	50	40	40	30	On	On	On	45	50	55	52	45	65
11 (10-11 am)	20	30	50	25	30	30	On	On	On	40	45	50	40	42	53
12 (11-12 pm)	20	30	30	25	25	30	On	On	On	45	50	50	51	60	60
13 (12-1 pm)	20	30	30	25	25	30	On	On	On	40	50	40	51	65	53
14 (1-2 pm)	20	30	20	25	25	20	On	On	On	35	45	40	51	65	51
15 (2-3 pm)	20	30	20	25	25	20	On	On	On	30	40	30	51	65	50
16 (3-4 pm)	30	30	20	25	25	20	On	On	On	30	40	30	51	65	44
17 (4-5 pm)	50	30	30	25	25	20	On	On	On	30	35	30	63	65	64
18 (5-6 pm)	50	50	40	25	25	20	On	On	On	40	40	40	80	75	62
19 (6-7 pm)	50	60	40	60	60	50	On	On	On	55	55	50	86	80	65
20 (7-8 pm)	70	60	60	80	70	70	On	On	On	60	55	50	70	80	63
21 (8-9 pm)	70	60	60	90	70	80	On	On	On	50	50	40	70	75	63
22 (9-10 pm)	80	70	80	80	70	60	On	On	On	55	55	50	70	75	63
23 (10-11 pm)	90	70	80	60	60	50	On	On	On	45	40	40	45	55	40
24 (11-12 am)	90	70	80	30	30	30	On	On	On	25	30	20	45	55	40
Total/Day	1390	1390	1300	855	785	810	2400	2400	2400	915	930	900	1217	1303	1287
Total/Week		96.40	0 hours		58.7	0 hours		168.	0 hours		64.0	5 hours		86.7	5 hours
Total/Year		5020	6 hours		306	1 hours		876	0 hours		334	0 hours		452	3 hours

Wk = Weekday

Hour of Day (Time)	O P Max	hedule ccupan ercent imum L	cy : Of	Lightir Po Max	hedule ng Rece e <b>rcen</b> f imum L	ptacle of	HV	hedule f AC Syst		Servi P Max	hedule ce Hot \ ercent timum L	Water t Of	P Max	hedule Elevator <b>ercent</b> timum L	of
	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun
1 (12-1 am)	0	0	0	5	5	5	Off	Off	Off	5	5	4	0	0	0
2 (1-2 am)	0	0	0	5	5	5	Off	Off	Off	5	5	4	0	0	0
3 (2-3 am)	0	0	0	5	5	5	Off	Off	Off	5	5	4	0	0	0
4 (3-4 am)	0	0	0	5	5	5	Off	Off	Off	5	5	4	0	0	0
5 (4-5 am)	0	0	0	5	5	5	Off	Off	Off	5	5	4	0	0	0
6 (5-6 am)	0	0	0	10	5	5	Off	Off	Off	8	8	7	0	0	0
7 (6-7 am)	10	10	5	10	10	5	On	On	Off	7	7	4	0	0	0
8 (7-8 am)	20	10	5	30	10	5	On	On	Off	19	11	4	35	16	0
9 (8-9 am)	95	30	5	90	30	5	On	On	Off	35	15	4	69	14	0
10 (9-10 am)	95	30	5	90	30	5	On	On	Off	38	21	4	43	21	0
11 (10-11 am)	95	30	5	90	30	5	On	On	Off	39	19	4	37	18	0
12 (11-12 pm)	95	30	5	90	30	5	On	On	Off	47	23	6	43	25	0
13 (12-1 pm)	50	10	5	80	15	5	On	On	Off	57	20	6	58	21	0
14 (1-2 pm)	95	10	5	90	15	5	On	On	Off	54	19	9	48	13	0
15 (2-3 pm)	95	10	5	90	15	5	On	On	Off	34	15	6	37	8	0
16 (3-4 pm)	95	10	5	90	15	5	On	On	Off	33	12	4	37	4	0
17 (4-5 pm)	95	10	5	90	15	5	On	On	Off	44	14	4	46	5	0
18 (5-6 pm)	30	5	5	50	5	5	On	On	Off	26	7	4	62	6	0
19 (6-7 pm)	10	5	0	30	5	5	On	Off	Off	21	7	4	20	0	0
20 (7-8 pm)	10	0	0	30	5	5	On	Off	Off	15	7	4	12	0	0
21 (8-9 pm)	10	0	0	20	5	5	On	Off	Off	17	7	4	4	0	0
22 (9-10 pm)	10	0	0	20	5	5	On	Off	Off	8	9	7	4	0	0
23 (10-11 pm)	5	0	0	10	5	5	Off	Off	Off	5	5	4	0	0	0
24 (11-12 am)	5	0	0	5	5	5	Off	Off	Off	5	5	4	0	0	0
Total/Day	920	200	60	1040	280	120	1600	1200	0	537	256	113	555	151	0
Total/Week		48.6	0 hours		56.0	0 hours		92.00	) hours		30.5	4 hours		29.2	5 hours
Total/Year		253	4 hours		292	0 hours		479	7 hours		159	2 hours		152	6 hours

# TABLE B103(4)LIGHT MANUFACTURING OCCUPANCY<sup>a</sup>

Wk = Weekday

#### TABLE B103(5) OFFICE OCCUPANCY<sup>a</sup>

Hour of Day (Time)	O P Max	hedule ccupan ercent imum L	cy of	Lightir Po Max	hedule ng Rece ercent imum L	ptacle of	HV	hedule AC Syst		Servi P Max	hedule ce Hot V ercent timum L	Water of oad	P Max	hedule Elevato ercent timum L	r Of .oad
	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun
1 (12-1 am)	0	0	0	5	5	5	Off	Off	Off	5	5	4	0	0	0
2 (1-2 am)	0	0	0	5	5	5	Off	Off	Off	5	5	4	0	0	0
3 (2-3 am)	0	0	0	5	5	5	Off	Off	Off	5	5	4	0	0	0
4 (3-4 am)	0	0	0	5	5	5	Off	Off	Off	5	5	4	0	0	0
5 (4-5 am)	0	0	0	5	5	5	Off	Off	Off	5	5	4	0	0	0
6 (5-6 am)	0	0	0	10	5	5	Off	Off	Off	8	8	7	0	0	0
7 (6-7 am)	10	10	5	10	10	5	On	On	Off	7	7	4	0	0	0
8 (7-8 am)	20	10	5	30	10	5	On	On	Off	19	11	4	35	16	0
9 (8-9 am)	95	30	5	90	30	5	On	On	Off	35	15	4	69	14	0
10 (9-10 am)	95	30	5	90	30	5	On	On	Off	38	21	4	43	21	0
11 (10-11 am)	95	30	5	90	30	5	On	On	Off	39	19	4	37	18	0
12 (11-12 pm)	95	30	5	90	30	5	On	On	Off	47	23	6	43	25	0
13 (12-1 pm)	50	10	5	80	15	5	On	On	Off	57	20	6	58	21	0
14 (1-2 pm)	95	10	5	90	15	5	On	On	Off	54	19	9	48	13	0
15 (2-3 pm)	95	10	5	90	15	5	On	On	Off	34	15	6	37	8	0
16 (3-4 pm)	95	10	5	90	15	5	On	On	Off	33	12	4	37	4	0
17 (4-5 pm)	95	10	5	90	15	5	On	On	Off	44	14	4	46	5	0
18 (5-6 pm)	30	5	5	50	5	5	On	On	Off	26	7	4	62	6	0
19 (6-7 pm)	10	5	0	30	5	5	On	Off	Off	21	7	4	20	0	0
20 (7-8 pm)	10	0	0	30	5	5	On	Off	Off	15	7	4	12	0	0
21 (8-9 pm)	10	0	0	20	5	5	On	Off	Off	17	7	4	4	0	0
22 (9-10 pm)	10	0	0	20	5	5	On	Off	Off	8	9	7	4	0	0
23 (10-11 pm)	5	0	0	10	5	5	Off	Off	Off	5	5	4	0	0	0
24 (11-12 am)	5	0	0	5	5	5	Off	Off	Off	5	5	4	0	0	0
Total/Day	920	200	60	1040	280	120	1600	1200	0	537	256	113	555	151	0
Total/Week		48.6	0 hours		56.0	0 hours		92.00	0 hours		30.5	4 hours		29.2	6 hours
Total/Year	Vaaleday		4 hours		292	0 hours		479′	7 hours		159	2 hours		152	6 hours

Wk = Weekday

# TABLE B103(6) PARKING GARAGE OCCUPANCY<sup>a</sup>

Hour of Day (Time)	O P	hedule ccupan e <b>rcen</b> t imum L	cy t <b>O</b> f	Lightir P	hedule ng Rece ercent imum L	ptacle Of		chedule AC Syst		Servi P	hedule ce Hot V ercent	Water t of	Р	hedule Elevato ercent	r t of
	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun
1 (12-1 am)				100	100	100									
2 (1-2 am)				100	100	100									
3 (2-3 am)				100	100	100									
4 (3-4 am)				100	100	100									
5 (4-5 am)				100	100	100									
6 (5-6 am)				100	100	100									
7 (6-7 am)				100	100	100									
8 (7-8 am)				100	100	100									
9 (8-9 am)				100	100	100									
10 (9-10 am)				100	100	100									
11 (10-11 am)				100	100	100	]	Based of	n				Inc	cluded w	vith
12 (11-12 pm)		NA		100	100	100	1	likely us	e		NA		other	coccupa	incies
13 (12-1 pm)				100	100	100									
14 (1-2 pm)				100	100	100									
15 (2-3 pm)				100	100	100									
16 (3-4 pm)				100	100	100									
17 (4-5 pm)				100	100	100									
18 (5-6 pm)				100	100	100									
19 (6-7 pm)				100	100	100									
20 (7-8 pm)				100 100	100	100									
21 (8-9 pm) 22 (9-10 pm)				100	$\begin{array}{c} 100 \\ 100 \end{array}$	100 100									
22 (9-10 pm) 23 (10-11 pm)				100	100	100									
23 (10-11 pm) 24 (11-12 am)				100	100	100									
24 (11-12 am)				100	100	100									
Total/Day				2400	2400	2400									
Total/Week					16	8 hours									
Total/Year					876	) hours									

Wk = Weekday

# TABLE B103(7) RESTAURANT OCCUPANCY<sup>a</sup>

Hour of Day (Time)	O P	hedule ccupan ercent imum L	cy t Of	Lightii P	hedule ng Rece <b>ercent</b> imum L	ptacle of		hedule AC Syst	-	Servi P	hedule ice Hot ercent cimum L	Water t Of	P	hedule Elevat ercer	or nt of
	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun
1 (12-1 am)	15	30	20	15	20	20	On	On	On	20	20	25	0	0	0
2 (1-2 am)	15	25	20	15	15	15	On	On	On	15	15	20	0	0	0
3 (2-3 am)	5	5	5	15	15	15	On	On	On	15	15	20	0	0	0
4 (3-4 am)	0	0	0	15	15	15	Off	Off	Off	0	0	0	0	0	0
5 (4-5 am)	0	0	0	15	15	15	Off	Off	Off	0	0	0	0	0	0
6 (5-6 am)	0	0	0	20	15	15	Off	Off	Off	0	0	0	0	0	0
7 (6-7 am)	0	0	0	40	30	30	Off	Off	Off	0	0	0	0	0	0
8 (7-8 am)	5	0	0	40	30	30	On	Off	Off	60	0	0	0	0	0
9 (8-9 am)	5	0	0	60	60	50	On	Off	Off	55	0	0	0	0	0
10 (9-10 am)	5	5	0	60	60	50	On	On	Off	45	50	0	0	0	0
11 (10-11 am)	20	20	10	90	80	70	On	On	On	40	45	50	0	0	0
12 (11-12 pm)	50	45	20	90	80	70	On	On	On	45	50	50	0	0	0
13 (12-1 pm)	80	50	25	90	80	70	On	On	On	40	50	40	0	0	0
14 (1-2 pm)	70	50	25	90	80	70	On	On	On	35	45	40	0	0	0
15 (2-3 pm)	40	35	15	90	80	70	On	On	On	30	40	30	0	0	0
16 (3-4 pm)	20	30	20	90	80	70	On	On	On	30	40	30	0	0	0
17 (4-5 pm)	25	30	25	90	80	60	On	On	On	30	35	30	0	0	0
18 (5-6 pm)	50	30	35	90	90	60	On	On	On	40	40	40	0	0	0
19 (6-7 pm)	80	70	55	90	90	60	On	On	On	55	55	50	0	0	0
20 (7-8 pm)	80	90	65	90	90	60	On	On	On	60	55	50	0	0	0
21 (8-9 pm)	80	70	70	90	90	60	On	On	On	50	50	40	0	0	0
22 (9-10 pm)	50	65	35	90	90	60	On	On	On	55	55	50	0	0	0
23 (10-11 pm)	35	55	20	50	50	50	On	On	On	45	40	40	0	0	0
24 (11-12 am)	20	35	20	30	30	30	On	On	On	25	30	20	0	0	0
Total/Day	750	740	485	1455	1365	1115	2000	1800	1700	790	730	625	0	0	0
Total/Week		49.7	5 hours		97.5	5 hours		13	5 hours		53.0	5 hours			0 hours
Total/Year		259	4 hours		508	6 hours		703	9 hours		276	6 hours			0 hours

Wk = Weekday

#### TABLE B103(8) RETAIL OCCUPANCY<sup>a</sup>

Hour of Day (Time)	Oc Po	hedule ccupane e <b>rcent</b> imum L	cy t Of	Lightin Po	hedule ng Rece e <b>rcen</b> f imum L	ptacle of		hedule AC Syst		Servi P	hedule ce Hot V ercent timum L	Water t Of	Р	hedule Elevato <b>ercen</b> t	r t of
	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun
1 (12-1 am)	0	0	0	5	5	5	Off	Off	Off	4	11	7	0	0	0
2 (1-2 am)	0	0	0	5	5	5	Off	Off	Off	5	10	7	0	0	0
3 (2-3 am)	0	0	0	5	5	5	Off	Off	Off	5	8	7	0	0	0
4 (3-4 am)	0	0	0	5	5	5	Off	Off	Off	4	6	6	0	0	0
5 (4-5 am)	0	0	0	5	5	5	Off	Off	Off	4	6	6	0	0	0
6 (5-6 am)	0	0	0	5	5	5	Off	Off	Off	4	6	6	0	0	0
7 (6-7 am)	0	0	0	5	5	5	On	On	Off	4	7	7	0	0	0
8 (7-8 am)	10	10	0	20	10	5	On	On	Off	15	20	10	12	9	0
9 (8-9 am)	20	20	0	50	30	10	On	On	On	23	24	12	22	21	0
10 (9-10 am)	50	50	10	90	60	10	On	On	On	32	27	14	64	56	11
11 (10-11 am)	50	60	20	90	90	40	On	On	On	41	42	29	74	66	13
12 (11-12 pm)	70	80	20	90	90	40	On	On	On	57	54	31	68	68	35
13 (12-1 pm)	70	80	40	90	90	60	On	On	On	62	59	36	68	68	37
14 (1-2 pm)	70	80	40	90	90	60	On	On	On	61	60	36	71	69	37
15 (2-3 pm)	70	80	40	90	90	60	On	On	On	50	49	34	72	70	39
16 (3-4 pm)	80	80	40	90	90	60	On	On	On	45	48	35	72	69	41
17 (4-5 pm)	70	80	40	90	90	60	On	On	On	46	47	37	73	66	38
18 (5-6 pm)	50	60	20	90	90	40	On	On	Off	47	46	34	68	58	34
19 (6-7 pm)	50	20	10	60	50	20	On	On	Off	42	44	25	68	47	3
20 (7-8 pm)	30	20	0	60	30	5	On	On	Off	34	36	27	58	43	0
21 (8-9 pm)	30	20	0	50	30	5	On	On	Off	33	29	21	54	43	0
22 (9-10 pm)	0	10	0	20	10	5	Off	On	Off	23	22	16	0	8	0
23 (10-11 pm)	0	0	0	5	5	5	Off	Off	Off	13	16	10	0	0	0
24 (11-12 am)	0	0	0	5	5	5	Off	Off	Off	8	13	6	0	0	0
Total/Day	720	750	280	1115	985	525	1500	1600	900	662	690	459	844	761	288
Total/Week		46.3	0 hours		70.8	5 hours		100	) hours		44.5	9 hours		52.6	9 hours
Total/Year		241	4 hours		369	4 hours		5214	4 hours		232	5 hours		274	7 hours

Wk = Weekday

#### TABLE B103(9) SCHOOL OCCUPANCY<sup>a</sup>

Hour of Day (Time)	Oc Pe Max	hedule ccupane ercent imum L	cy Of .oad	Lightii Pe Max	hedule ng Rece ercent imum L	ptacle Of oad	HV	hedule AC Syst	em	Servi Pe Max	hedule ce Hot ercent imum L	Water Of Load	Pe Max	hedule Elevato ercent timum L	r Of .oad
	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun
1 (12-1 am)	0	0	0	5	5	5	Off	Off	Off	5	3	3	0	0	0
2 (1-2 am)	0	0	0	5	5	5	Off	Off	Off	5	3	3	0	0	0
3 (2-3 am)	0	0	0	5	5	5	Off	Off	Off	5	3	3	0	0	0
4 (3-4 am)	0	0	0	5	5	5	Off	Off	Off	5	3	3	0	0	0
5 (4-5 am)	0	0	0	5	5	5	Off	Off	Off	5	3	3	0	0	0
6 (5-6 am)	0	0	0	5	5	5	Off	Off	Off	5	3	3	0	0	0
7 (6-7 am)	0	0	0	5	5	5	Off	Off	Off	5	3	3	0	0	0
8 (7-8 am)	5	0	0	30	5	5	On	Off	Off	10	3	3	0	0	0
9 (8-9 am)	75	10	0	85	15	5	On	On	Off	34	3	5	30	0	0
10 (9-10 am)	90	10	0	95	15	5	On	On	Off	60	5	5	30	0	0
11 (10-11 am)	90	10	0	95	15	5	On	On	Off	63	5	5	30	0	0
12 (11-12 pm)	80	10	0	95	15	5	On	On	Off	72	5	5	30	0	0
13 (12-1 pm)	80	10	0	80	15	5	On	On	Off	79	5	5	30	0	0
14 (1-2 pm)	80	0	0	80	5	5	On	Off	Off	83	3	5	30	0	0
15 (2-3 pm)	80	0	0	80	5	5	On	Off	Off	61	3	3	30	0	0
16 (3-4 pm)	45	0	0	70	5	5	On	Off	Off	65	3	3	15	0	0
17 (4-5 pm)	15	0	0	50	5	5	On	Off	Off	10	3	3	0	0	0
18 (5-6 pm)	5	0	0	50	5	5	On	Off	Off	10	3	3	0	0	0
19 (6-7 pm)	15	0	0	35	5	5	On	Off	Off	19	3	3	0	0	0
20 (7-8 pm)	20	0	0	35	5	5	On	Off	Off	25	3	3	0	0	0
21 (8-9 pm)	20	0	0	35	5	5	On	Off	Off	22	3	3	0	0	0
22 (9-10 pm)	10	0	0	30	5	5	On	Off	Off	22	3	3	0	0	0
23 (10-11 pm)	0	0	0	5	5	5	Off	Off	Off	12	3	3	0	0	0
24 (11-12 am)	0	0	0	5	5	5	Off	Off	Off	9	3	3	0	0	0
Total/Day	710	50	0	990	170	120	1500	500	0	691	80	84	285	0	0
Total/Week		36.0	0 hours		52.4	0 hours		80.0	0 hours		36.1	9 hours		14.2	5 hours
Total/Year		187	7 hours		273	2 hours		417	1 hours		188	7 hours		74	3 hours

Wk = Weekday

## TABLE B103(10) WAREHOUSE OCCUPANCY<sup>a</sup>

Hour of Day (Time)	Oc Po Max	hedule ccupane e <b>rcent</b> imum L	cy Of oad	Lightii P Max	hedule ng Rece ercent imum L	ptacle Of oad	HV	hedule AC Syst	tem	Servi P Max	hedule ce Hot <b>ercen</b> t timum L	Water t Of Load	P Max	hedule Elevato <b>ercen</b> t timum L	r t Of .oad
	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun	Wk	Sat	Sun
1 (12-1 am)	0	0	0	5	5	5	Off	Off	Off	2	2	2	0	0	0
2 (1-2 am)	0	0	0	5	5	5	Off	Off	Off	2	2	2	0	0	0
3 (2-3 am)	0	0	0	5	5	5	Off	Off	Off	2	2	2	0	0	0
4 (3-4 am)	0	0	0	5	5	5	Off	Off	Off	2	2	2	0	0	0
5 (4-5 am)	0	0	0	5	5	5	Off	Off	Off	5	2	2	0	0	0
6 (5-6 am)	0	0	0	5	5	5	Off	Off	Off	7	2	2	0	0	0
7 (6-7 am)	0	0	0	5	5	5	Off	Off	Off	7	2	2	0	0	0
8 (7-8 am)	15	0	0	40	5	5	On	Off	Off	10	2	2	0	0	0
9 (8-9 am)	70	20	0	70	8	5	On	On	Off	30	6	2	0	0	0
10 (9-10 am)	90	20	0	90	24	5	On	On	Off	36	12	2	0	0	0
11 (10-11 am)	90	20	0	90	24	5	On	On	Off	36	12	2	30	0	0
12 (11-12 pm)	90	20	0	90	24	5	On	On	Off	46	17	2	0	0	0
13 (12-1 pm)	50	10	0	80	5	5	On	On	Off	57	4	4	0	0	0
14 (1-2 pm)	85	10	0	90	5	5	On	On	Off	43	4	4	0	0	0
15 (2-3 pm)	85	10	0	90	5	5	On	On	Off	38	2	2	0	0	0
16 (3-4 pm)	85	10	0	90	5	5	On	On	Off	40	2	2	40	0	0
17 (4-5 pm)	20	0	0	90	5	5	On	Off	Off	30	2	2	0	0	0
18 (5-6 pm)	0	0	0	30	5	5	Off	Off	Off	18	2	2	0	0	0
19 (6-7 pm)	0	0	0	5	5	5	Off	Off	Off	3	2	2	0	0	0
20 (7-8 pm)	0	0	0	5	5	5	Off	Off	Off	3	2	2	0	0	0
21 (8-9 pm)	0	0	0	5	5	5	Off	Off	Off	3	2	2	0	0	0
22 (9-10 pm)	0	0	0	5	5	5	Off	Off	Off	3	2	2	0	0	0
23 (10-11 pm)	0	0	0	5	5	5	Off	Off	Off	3	2	2	0	0	0
24 (11-12 am)	0	0	0	5	5	5	Off	Off	Off	3	2	2	0	0	0
Total/Day	680	120	0	915	180	120	1000	800	0	429	91	52	70	0	0
Total/Week		35.2	0 hours		48.7	5 hours		58.0	0 hours		22.8	8 hours		3.5	0 hours
Total/Year	1	183	5 hours		254	2 hours		302	4 hours		119	3 hours		18	2 hours

Wk = Weekday

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# **APPENDIX C**

# **EXTERIOR DESIGN CONDITIONS**

As required by Sections C302.2 and R302.2, the heating or cooling outdoor design temperatures shall be selected from Table C-1.

Location	Outdoor Design Temp Heating (°F)	Outdoor Design Temp Cooling (°F)
Aberdeen 20NNE	25	83
Anacortes	24	72
Anatone	-4	89
Auburn	25	84
Battleground	19	91
Bellevue	24	83
Bellingham 2N	19	78
Blain	17	73
Bremerton	29	83
Burlington	19	77
Chehalis	21	87
Chelan	10	89
Cheney	4	94
Chesaw	-11	81
Clarkston	10	94
Cle Elum	1	91
Colfax 1NW	2	94
Colville AP	-2	92
Concrete	19	83
Connell 4NNW	6	100
Cougar 5E	25	93
Dallesport AP	14	99
Darrington RS	13	85
Davenport	5	92
Edmonds	24	82
Ellensburg AP	2	90
Elma	24	88
Ephrata AP	7	97
Everett Paine AFB	21	79
Forks 1E	23	81
Glacier RS	13	82
Glenoma (Kosmos)	18	89
Goldendale	7	94
Grays River Hatchery	24	86

# TABLE C-1 OUTDOOR DESIGN TEMPERATURES

\_\_\_\_\_

Location	Outdoor Design Temp Heating (°F)	Outdoor Design Temp Cooling (°F)
Greenwater	1.4	84
Grotto	21	84
Hoquiam AP	26	79
Inchelium 2NW	0	92
John Day Dam	19	100
Long Beach 3NNE	25	77
Longview	24	87
Lower Granite Dam	14	98
Lower Monument Dam	18	103
Marysville	23	79
Metaline Falls	-1	89
Methow 2W	1	89
Nespelem 2S	-4	93
Newhalem	19	89
Newport	-5	92
Northport	2	92
Oak Harbor	16	74
Odessa	7	100
Olga 2SE	24	71
Olympia AP	17	85
Omak 2NW	3	90
Oroville	5	93
Othello	9	98
Packwood	16	90
Plain	-3	89
Pleasant View	16	98
Pomeroy	3	95
Port Angeles	28	75
Port Townsend	25	76
Prosser	12	97
Puyallup	19	86
Quilcene 2SW	23	83
Quinault RS	25	84

Location	Outdoor Design Temp Heating (°F)	Outdoor Design Temp Cooling (°F)
Rainier, Longmire	15	85
Paradise RS	8	71
Raymond	28	81
Redmond	17	83
Republic	-9	87
Richland	11	101
Ritzville	6	99
Satus Pass	10	90
Seattle: SeaTac AP	24	83
Sedro Woolley 1E	19	78
Sequim	23	78
Shelton	23	85
Smyrna	8	102
Snohomish	21	81
Snoqualmie Pass	6	80
Spokane AP	4	92
Spokane CO	10	96
Stampede Pass	7	76
Stehekin 3 NW	12	85
Stevens Pass	6	77
Tacoma CO	29	82
Tatoosh Island	31	63
Toledo AP	17	84
Vancouver	22	88
Vashon Island	28	78
Walla Walla AP	6	96
Waterville	1	88
Wellpinit	1	93
Wenatchee CO	10	92
Whidbey Island	11	71
Willapa Harbor	26	81
Wilson Creek	3	96
Winthrop 1WSW	-12	91
Yakima AP	11	94

**ABBREVIATIONS:** Typical: "4(miles)NE"

AFB Air Force Base

AP Airport

CO City Office

**RS** Ranger Station

# APPENDIX D RENEWABLE ENERGY

**D101.1 On-site renewable energy systems.** Each new commercial building or addition larger than 5,000 square feet of gross conditioned floor area shall include a renewable energy generation system consisting of at least 70 watts rated peak photovoltaic energy production, or 240 kBtu of annual solar water heating energy production, per 1,000 square feet of conditioned floor area or fraction thereof. For buildings over 5 stories in height, the conditioned area for this calculation shall be based on the conditioned area of the largest 5 above-grade stories in the building. If the on-site renewable energy option in C406 is selected, this energy shall be in addition to that required by C406.

**Exception**: Alternate means of achieving equivalent energy savings are permissible where approved by the code official, if the calculated net annual energy savings equals or exceeds the calculated annual energy production of the required on-site renewable energy system.